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ANALYSIS OF CONSTANT PHASE CONTOURS OF  
EVAPORATION DUCT MODE FUNCTIONS  
FOR WAVEGUIDE MODE PROPAGATION

by

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Submitted in partial fulfillment  
of the requirements for the degree of

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## ABSTRACT

The M-Layer program tracks the constant phase lines  $\text{Im}\{D(q)\} = 0$  and looks for their intersections with the lines  $\text{Re}\{D(q)\} = 0$  for the locations of the zeros of the mode function  $D(q)$ . These two types of constant phase lines are tracked and plotted over a search region which contains modes having a range attenuation rate of no more than 5 dB per km. Several new parameters for use in mode search are deduced from the results and some old ones are verified. Future studies in waveguide mode propagation theory pertaining to atmospheric ducts may benefit from this work. An improved mode search strategy is also proposed.

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## TABLE OF CONTENTS

I. INTRODUCTION .....	1
A. THE WAVEGUIDE MODE THEORY OF PROPAGATION .....	2
B. MODE SEARCH PRINCIPLE .....	7
II. MODE FUNCTION IN THE COMPLEX $q_{11}/t_1$ PLANE .....	11
A. MODE LOCATIONS .....	11
B. PHASE LINE TRACKING .....	13
1. Downward Tracking .....	13
2. Upward Tracking .....	18
III. ANALYSIS AND CONCLUSIONS .....	21
A. MODE SEARCH PARAMETERS .....	21
B. MODE SEARCH STRATEGY .....	24
1. Track Termination .....	24
2. Search Termination .....	25
3. Track Duplication Avoidance .....	27
APPENDIX A: MODE LOCATIONS IN THE COMPLEX $q_{11}/t_1$ PLANE .....	28

APPENDIX B: SUBROUTINE FNDMOD AND FZEROX ..... 49

APPENDIX C: CONSTANT PHASE LINE TRACKING FLOW CHARTS ..... 61

APPENDIX D: CONSTANT PHASE LINES IN THE COMPLEX  $q_{11}/t_1$   
PLANE ..... 66

APPENDIX E: SEPARATION OF  $\text{Im}\{D(q)\}=0$  LINES ..... 75

APPENDIX F: DIFFERENCE BETWEEN CONSECUTIVE  $\text{Re}(q_m/t_1)$  VALUES 84

LIST OF REFERENCES ..... 93

INITIAL DISTRIBUTION LIST ..... 94

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## I. INTRODUCTION

The M-Layer program developed by NOSC (Naval Ocean System Center) was documented by Yeoh [Ref. 1] at NPS. It was later extensively revised by Lee and Han [Ref. 2] for improved accuracy and speed. The new FORTRAN code is now identified as the NPS version [Ref. 3] under the auspices of NRaD (Naval Command, Control and Ocean Surveillance Center, RDT&E Division), the current name for NOSC. In this version, the logical structures and numerical algorithms for following the constant phase lines of the mode function and for computing the mode locations were almost completely rewritten. The overall plan to first partition the search region into rectangular areas and then circulate around these rectangles to search for the modes, i.e., the mode search protocol, was left unchanged. Lee and Han [Ref. 2] recommended that a more direct mode search protocol should be devised to locate the modes more expediently. If possible, such an approach should locate the modes in the order of ascending range attenuation rates.

To design a more efficient mode search protocol, a better understanding of the mode function beyond the known locations of the modes is required. In this thesis, the analytical property of the mode function is investigated. Programs are written to track and plot the constant phase lines along which the mode function is either real or purely imaginary. From the results, a new strategy to locate the modes is recommended.

In the remainder of this chapter, the background theory and some of the notations used in this thesis are introduced. The basic theory presented in Sections A and B follows Ref. 3 closely. The results of this research are presented in Chapter II. In Chapter III, a new mode search protocol is proposed based on the findings of this thesis. The relevant parameters for use in this new approach are also discussed.

## A. THE WAVEGUIDE MODE THEORY OF PROPAGATION

Trapping of electromagnetic (EM) waves in the modes supported by a duct is the dominating factor in over-the-horizon propagation. The computer program M-Layer searches for these modes and computes the electric field from the Hertz vector. Assume a vertical electric dipole

$$\vec{J} = 4\pi z \delta(x) \delta(y) \delta(z - z_T)$$

at a height  $z = z_T$  above the surface of the earth. Following Freehafer [Ref. 4], the Hertz vector of the EM fields can be written, in the cylindrical coordinates  $(\rho, \phi, z)$ , as a sum of contributions from individual modes [Ref. 1]:

$$\Pi(\rho, z) = -\pi j \sum_m H_0^{(2)}(\beta_m \rho) g_m(z_T) g_m(z) \quad (1)$$

where  $\beta_m$  is the wavenumber of the  $m$ -th mode and is independent of the coordinates;  $z_T$  is the height of the transmitter above the ground,  $H_0^{(2)}$  is the Hankel function of the second kind, which represents an outgoing wave in the radial direction when the time

dependence  $e^{j\omega t}$  is adopted, and  $g_m$  is the height-gain function of the  $m$ -th mode, normalized so that the integral of its square over all heights equals unity when either an electric or a magnetic dipole source is used. The height-gain function satisfies the equation

$$\left( \frac{\partial^2}{\partial z^2} + k^2 m^2(z) - \beta_m^2 \right) g_m(z) = 0 \quad (2)$$

where  $k$  is the free-space wavenumber,  $m(z)$  is the modified index of refraction, and  $m^2(z)$  is approximated with a continuous, piecewise linear profile having  $I$  layers:

$$m^2(z) = m_i^2 + \alpha_i(z - z_i) \quad z_i \leq z \leq z_{i+1}, \quad 1 \leq i \leq I. \quad (3)$$

In practice,  $m(z)$  deviates only slightly from unity in the troposphere. The modified refractivity  $M(z) = [m(z) - 1] \times 10^6$ , as shown in Fig. 1, is commonly used. The slope of  $M(z)$  is approximately  $\alpha_i \times 10^6/2$ .

In the  $i$ -th layer, the height-gain function is given by

$$g_m(z) = B_i(\beta_m) [C_i(\beta_m) k_1(q_{mi}) + k_2(q_{mi})] \quad z_i \leq z \leq z_{i+1} \quad (4)$$

where  $q_{mi}$  is a dimensionless linear function of height  $z$  with  $k$ ,  $\beta_m$ ,  $m_i$ , and  $\alpha_i$  as parameters:

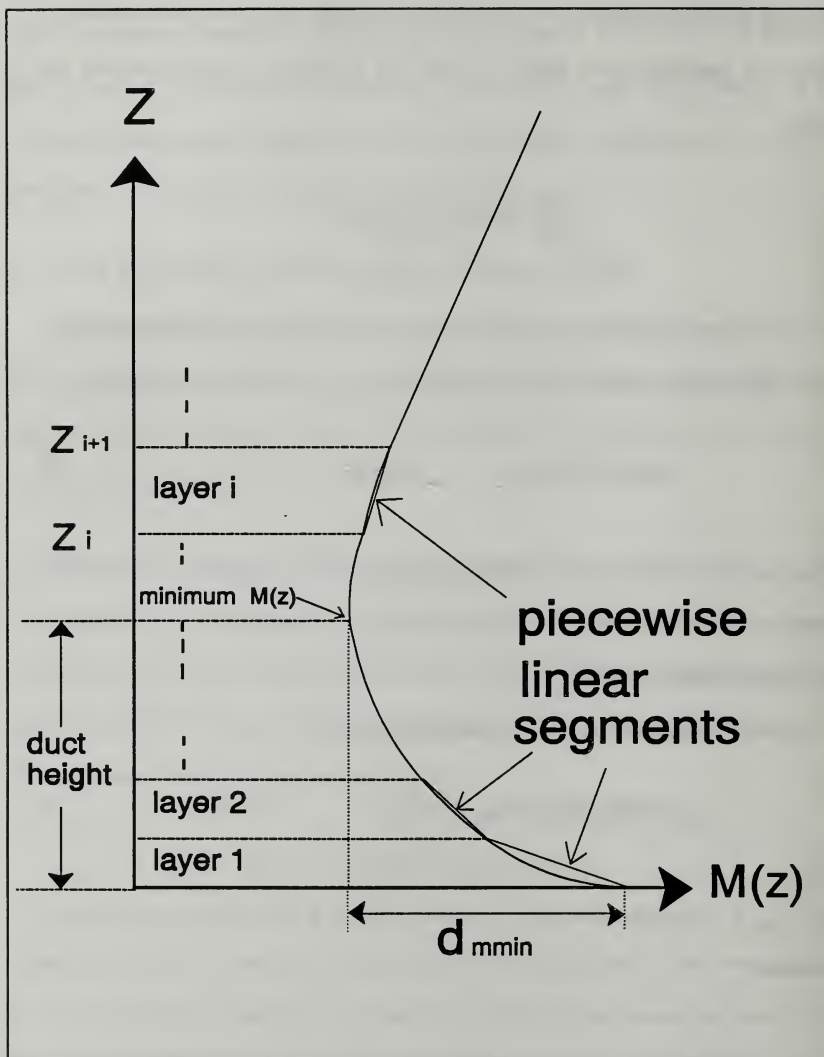


Figure 1. Typical modified refractivity  $M(z)$  profile.



$$q_{mi} = \sqrt[3]{\left(\frac{k}{\alpha_i}\right)^2 \left(m_i^2 + \alpha_i(z-z_i) - \frac{\beta_m^2}{k^2}\right)} \quad (5)$$

The functions  $k_1(q_{mi})$  and  $k_2(q_{mi})$  are given in terms of the Airy function  $Ai$ :

$$k_1(q_{mi}) = -j2(12)^{1/6} Ai(-q_{mi} e^{j2\pi/3}) \quad (6)$$

and

$$k_2(q_{mi}) = 2(12)^{1/6} Ai(-q_{mi}). \quad (7)$$

For  $z > z_{I+1}$ ,  $m^2(z)$  is extended continuously upward at a constant slope commensurate with the effective radius of the earth. This slope equals  $2.36 \times 10^{-7} \text{ (m}^{-1}\text{)}$  for the four-thirds effective earth radius model. Thus, the height-gain function  $g_m$  is again given by Eqs. (4) through (7) for  $z > z_{I+1}$ , with the constant  $C_{I+1}$  set to  $e^{j4\pi/3}$  to represent an upward going wave as  $z$  becomes large. Beneath the "flattened" earth surface where  $z < z_1 = 0$ ,  $m^2(z)$  is deduced from the dielectric constant and the conductivity of sea water, which are set to 80.8869 and 4.64 (Si/m) respectively. Here the Hertz vector is represented by a downward propagating plane wave in this region.

The conditions that the tangential components of the electric and magnetic fields are continuous across the layer boundaries determine the coefficients  $C_i$ . Starting from the top layer down, or "integration-down" [Ref. 1], every  $C_i$  is uniquely determined by  $C_{i+1}$  at  $z = z_{i+1}$ . Thus, a set of all  $C_i$  coefficients is determined without considering the boundary conditions at  $z = z_1$ . On the other hand, starting from the lowest boundary at

$z = z_1$  up to  $z = z_I$ , or "integration-up", a second set of  $C_i$  coefficients is determined without applying the boundary conditions at  $z = z_{I+1}$ . That these two sets of  $C_i$  coefficients are identical is a manifestation that  $\beta_m$  is the wavenumber of a mode. Mathematically, this consistency condition, sometimes called the guidance condition [Ref. 5], can be expressed as the vanishing of a determinant  $D$  called the mode function [Ref. 6]. The elements of this determinant consist of linear combinations of  $k_1(q_{mi})$  and  $k_2(q_{mi})$  and their derivatives with respect to height at the boundaries. The M-Layer program searches for the zeros of the mode function to find the wavenumbers. Once a wavenumber is obtained, the height-gain function of the corresponding mode can be computed. Note that the normalization condition on  $g_m$  and the boundary conditions, together with the  $C_i$  coefficients, determine the  $B_i$  coefficients to within an overall sign. This sign need not be resolved because only products in the form of  $g_m(z)g_m(z_T)$  from each mode contribute to the Hertz vector.

Since the mode function  $D$  depends on the wavenumber  $\beta_m$  only through the values of  $q_{mi}$  at the layer boundaries, it is more convenient to consider  $D$  as a function of the variable  $q$  given by

$$q = \sqrt[3]{\left(\frac{k}{\alpha_1}\right)^2 \left(m_1^2 - \frac{\beta^2}{k^2}\right)}, \quad (8)$$

and to search for the zeros of  $D(q)$  in the complex  $q$  plane. The  $m$ -th zero is designated as  $q_m$  and is called a  $q$ -eigenvalue and  $\beta_m$  is then deduced from  $q_m$  by inverting Eq. (8)

for  $\beta$ . In the NPS version,  $q_m$  is ordered in ascending attenuation rate of the mode, which is approximately proportional to the imaginary part of  $\beta_m$ .

## B. MODE SEARCH PRINCIPLE

M-Layer searches for modes which have attenuation rates below a specified value. At ground ranges more than several wavelengths away, this attenuation rate is proportional to the imaginary part of the wavenumber  $\beta_m$  as can be seen from Eq. (1). In the upper complex  $q$  plane, for values of  $q$  such that

$$\left| q \left( \frac{k}{\alpha_1} \right)^{-2\beta} \right| = \left| m_1^2 - \frac{\beta^2}{k^2} \right| < 1, \quad (9)$$

$m_1 - \beta/k$  is approximately proportional to  $q$  because the absolute value of  $m_1$  and, hence, that of  $\beta/k$ , are both nearly unity. Thus, the limit on attenuation rate imposed on the imaginary part of  $\beta$  can be translated approximately into an upper bound<sup>1</sup> on the imaginary part of  $q$  which defines a strip in the complex  $q$  plane called the search region. This region is covered with layers of identical square meshes whose sides are parallel to the imaginary  $q$  axis and have a length equivalent to an attenuation rate of  $1/32 \text{ dB}^2$  per

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<sup>1</sup> Since the absorption is small in air, the modified index of refraction  $m(z)$ , and hence  $\alpha_1$ , are considered as real quantities in the following discussions. In the actual FORTRAN code, they are declared as complex variables.

<sup>2</sup> This is the default value of the NPS version which can be adjusted through editing the variable "dmesh" in an ASCII input file.

kilometer. The lower edges of the meshes in the lowest layer sit along the real  $q$  axis<sup>3</sup>. The meshes in the layer just below the top one contain the upper bound of the search region, with the top layer providing some allowance for numerical inaccuracy. The program tests each mesh square for the presence of zeros of the mode function  $D(q)$ .

To search through all the meshes, the program first divides the mesh covering the search region into "contour rectangles" with equally spaced vertical lines parallel to the imaginary  $q$  axis. These vertical lines contain the edges of stacked square meshes and are separated by a distance 160 times the side of a mesh. The search commences at the top left corner and moves counterclockwise around each "contour rectangle" and begins with the one whose left edge is defined by

$$\operatorname{Re}\left[q\left(\frac{k}{\alpha_1}\right)^{-2\beta}\right]=\operatorname{Re}\left(m_1^2-m_{\min}^2\right) \approx 2 \times 10^{-6} \operatorname{Re}\left(M_1-M_{\min}\right)=2 \times 10^{-6} d_{\min}, \quad (10)$$

where  $m_{\min}$  is the minimum value of the modified index of refraction profile and  $d_{\min}$  is shown in Fig. 1. The justification for this choice to begin the mode search is as follows: From Eq. (5) and optics, for a wave to propagate freely in space, the dispersion relation of the Maxwell equations requires that  $k^2 m^2(z) > \beta_m^2$ , assuming that both quantities are real. Thus, the smallest  $\beta_m^2$  to support a trapped wave will occur when

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<sup>3</sup> The NOSC version extends the lower edge slightly below the real  $q$ -axis. This causes problems in some situations [Ref. 2].

$\beta_m^2$  just exceeds the minimum of  $m^2(z)$ <sup>4</sup>. It is not surprising that an argument based on optics works within a waveguide mode formulation which is low frequency in principle. Lee [Ref. 7] has demonstrated that the earth-flattening approximation actually links Mie's low frequency oriented spherical harmonics to Fock's high frequency diffraction theory through the uniform asymptotics. The mere introduction of an unlimited ground range into the Maxwell differential equations incorporates the global feature of the radius of the earth into the local equations.

After the search over the initial rectangle is completed, the program goes on to search the neighboring rectangle to the left. If a specified number<sup>5</sup> of consecutive rectangles of decreasing real  $q$  values have been searched without turning up any zero of  $D(q)$ , the program changes direction and starts to search the rectangles to the right of the initial "contour rectangle" one by one, with increasing real part of  $q$ . After failing consecutively to locate any  $q$ -eigenvalue again over the specified number of rectangles, the program assumes that no more zeros of  $D(q)$  exists in the search region. The mode search is considered complete and the procedure is terminated. If the array for storing the  $q$ -eigenvalues is filled up before the search is completed, the search is terminated with an error message.

---

<sup>4</sup> Note that assuming the same real part, an imaginary component of  $\beta_m$  reduces the real part of  $\beta_m^2$  which may enable the wave to propagate in the  $z$ -direction.

<sup>5</sup> This number of consecutive rectangles is an adjustable input variable "nstop" in the NPS version. The default value is 2.

The search for zeros of  $D(q)$  makes use of the fact that a real valued function changes sign when it crosses a simple zero. Since a zero of the complex valued function  $D(q)$  is where both its real part and imaginary part vanish, a necessary condition for a point  $q_m$  to be a zero is that it is the intersection of two curves defined by  $\text{Im}\{D(q)\} = 0$  and  $\text{Re}\{D(q)\} = 0$ . M-Layer moves along each side of a "contour rectangle" while searching for a sign change in  $\text{Im}\{D(q)\}$  across an edge of a mesh bordering the side of this rectangle to determine that a line of  $\text{Im}\{D(q)\} = 0$  has been encountered. The search then follows this line into the meshes within the "contour rectangle", checking each mesh to see if a curve  $\text{Re}\{D(q)\} = 0$  enters the mesh being inspected. All these steps make use of the assumption that the zeros of  $D(q)$  are simple. Once both the curve  $\text{Im}\{D(q)\} = 0$  and the curve  $\text{Re}\{D(q)\} = 0$  are found to be present within a mesh, the locations of their possible intersections are estimated.

The rule for sign change becomes inconclusive if a zero of  $\text{Im}\{D(q)\} = 0$  or if  $\text{Re}\{D(q)\} = 0$  happens to fall on a corner of a mesh, and a remedy is required. In the NPS version, whenever the real part or the imaginary part of  $D(q)$  vanishes on a corner of a mesh, the phase angle of  $D(q)$  is rotated by  $2^{-52}$  radians. This maneuver effectively shifts  $q$  by a small amount to resolve the sign ambiguity.

To estimate the locations of zeros of  $D(q)$  within a mesh,  $D(q)$  is assumed to be well approximated in this mesh by its four-term Taylor series expansion. The unshifted values of  $D(q)$  at the mesh corners determine this cubic polynomial uniquely. Cardan's formulas [Ref. 8] are used to locate the zeros of this polynomial before retaining only those lying within the mesh.



## II. MODE FUNCTION IN THE COMPLEX $q_{11}/t_1$ PLANE

### A. MODE LOCATIONS

M-Layer searches for the zeros of the mode function  $D(q)$  in the complex  $q$  plane by tracking the constant phase lines of  $D(q)$  along which the mode function is either real or purely imaginary. The zeros found are called the  $q$ -eigenvalues as defined by Eq. (8) and are denoted as  $q_m$ . These eigenvalues are saved in an ASCII file and are utilized later for height-gain function computations. In order to design a strategy for locating these zeros, the mode locations are plotted.

It is clear from Eq. (8) that the variable  $q$  varies with  $\alpha_1$ , the slope of  $m^2(z)$  in the lowest (first) layer. Since  $\alpha_1$  depends on how the continuous, piecewise linear approximation to  $m^2(z)$  is made, while both  $m_1$  and  $\beta_m$  are, in principle, dependent only on the actual profile,  $q$  will vary strongly with  $\alpha_1$  and fail to provide information on the wavenumber of the mode directly. A more suitable variable to use is, from Eq. (8):

$$q \left( \frac{k}{\alpha_1} \right)^{-2/3} = m_1^2 - \frac{\beta^2}{k^2}. \quad (11)$$

Since  $q$  is given the variable name of  $q_{11}$  and  $(k/\alpha_1)^{2/3}$  is given the variable name of  $t_1$  in the M-Layer FORTRAN code, this variable is identified as  $q_{11}/t_1$  throughout this thesis. Since  $m_1$  is real and both it and  $\beta/k$  deviate from unity only slightly for all cases

investigated,  $q_{11}/t_1$  is approximately  $2(m_1 - \beta/k)$ . Thus, its imaginary part is directly proportional to  $-\beta$ , the attenuation rate of the mode. Furthermore,  $q_{11}/t_1$  does not depend explicitly on  $\alpha_1$ . Removing the  $t_1$  factor from  $q_{11}$  makes it possible to compare results from different evaporation duct profiles meaningfully.

Plots of the  $q$ -eigenvalues as individual points in the complex  $q_{11}/t_1$  plane are included in Appendix A. For the 20 meter duct, which will be used as the representative case for discussions in this thesis, a line linking all the eigenvalues in the order of increasing attenuation rate is shown in Fig. 2. Because of the long excursion between

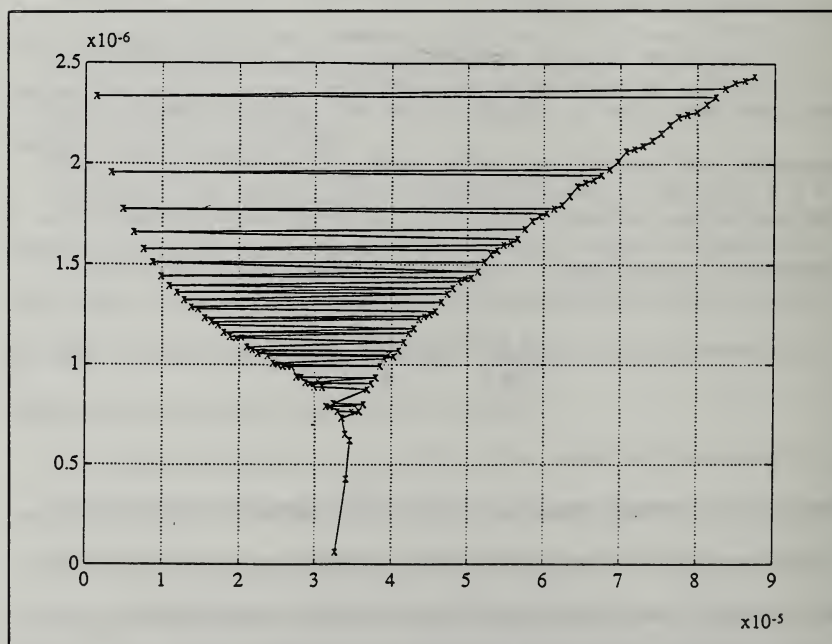


Figure 2.  $q$ -eigenvalues in the  $q_{11}/t_1$  plane, connected in the order of ascending attenuation rate (20 m duct).



many pairs of consecutive modes in the upper part of this figure, it appears that the intuitive approach of starting with the mode of the lowest attenuation and continually looking for the mode with the next higher attenuation rate may not be the most efficient strategy. Furthermore, there seems to be a fork near the middle of the figure which suggests that there can be more than one constant phase line passing through all the zeros of the mode function. These problems suggest that, in order to design an efficient mode search strategy, the behavior of the mode function in the complex  $q_1/t_1$  plane has to be investigated more thoroughly.

## B. PHASE LINE TRACKING

The M-Layer program follows a line along which  $\text{Im}\{D(q)\} = 0$  until a zero is encountered at its intersection with another line along which  $\text{Re}\{D(q)\} = 0$ . Since there is no way to determine the phase of the constant phase line linking two adjacent zeros *a priori*, following these two types of somewhat arbitrary but easy to compute phase lines which have constant phases of 0 or  $\pi$ , and  $\pi/2$  or  $3\pi/2$ , respectively, are still the best way to program a computer to locate the zeros systematically. It is thus necessary to find out the actual distribution of these constant phase lines in the complex  $q_1/t_1$  plane.

### 1. Downward Tracking

In the original design, along the real  $q$  axis, M-Layer divides the search region into "contour rectangles," each of which spans 160 meshes horizontally. From the observed locations of the modes, it is found desirable to track and plot the constant phase lines along  $\text{Im}\{D(q)\} = 0$  and  $\text{Re}\{D(q)\} = 0$  over a little more than six "contour

rectangles", roughly three to the right and three to the left of the starting real  $q$  coordinate given by Eq. (10), which is a variable called  $q_{\text{test}}$  in M-Layer. The subroutine FNDMOD and FZEROX are modified to track these constant phase lines. A listing of these modified routines for tracking the lines  $\text{Im}\{D(q)\} = 0$  beginning from the top edge and moving downwards into the search region is included in Appendix B. Their flow charts are given in Appendix C. Only minor changes are required to track the type of lines  $\text{Re}\{D(q)\} = 0$ , or to track these lines from the bottom of the search region upwards. The program first searches for a sign change in  $\text{Im}\{D(q)\}$  or in  $\text{Re}\{D(q)\}$  along the top edge of the search region, starting at the coordinate -512 mesh sizes from  $q_{\text{test}}$ , until a distance of 1024 mesh sizes is covered. When a sign change is observed, a constant phase line is recognized as passing through the particular mesh square and the program writes the complex  $q$  value of the lower-left corner of this mesh square into an ASCII file identified by whether the mode function is real or imaginary along the line, and the order this line is found. The program then moves from the top edge downwards to follow this constant phase line until it exits the search region. The  $q$  values of the lower-left corner of the mesh squares along this phase line are also written into the same ASCII file to be plotted later using MATLAB/386. The constant phase lines for the mode functions of the 2, 4, 6, 8, 10, 20, 30 and 40 meter evaporation ducts are obtained and plotted. They are included in Appendix D. Tracking and plotting these constant phase lines are extremely time consuming. The CPU time required to track the desired constant phase lines for each duct using an Intel 80486 based PC running at a 33 MHz clock rate is listed in Table 1. The time required to plot those lines for each duct using an Intel 80386 based PC running

at a 16 MHz clock rate is also listed.

**TABLE 1**  
**CPU Time for Tracking and Plotting Constant Phase Lines**

duct height (m)	tracking $\text{Im}\{D(q)\} = 0$ (hr:min:sec)	tracking $\text{Re}\{D(q)\} = 0$ (hr:min:sec)	plotting both lines (hr:min:sec)
2	1:47:39	1:46:23	0:21:28
3	2:47:41	2:48:50	0:23:17
3	3:43:54	3:45:11	0:25:42
8	4:25:49	4:23:41	0:29:34
10	6:08:14	6:11:03	0:32:25
20	8:26:58	8:24:22	0:34:21
30	9:08:14	9:06:45	0:36:49
40	8:39:04	8:37:54	0:36:53
Total	45:07:33	45:04:09	4:01:29

The constant phase line plot for the mode function of the 20 m evaporation duct is given in Fig. 3. The solid lines represent those having  $\text{Im}\{D(q)\} = 0$ ; the dotted lines represent those having  $\text{Re}\{D(q)\} = 0$ . Every intersection of these two types of phase lines is the location of a  $q$ -eigenvalue scaled by  $t_1$ , thus indicating the presence of a mode. Note that every solid line intersects with a dotted line except for many of those running from the top through the bottom of the search region. None of the solid lines intersect with other solid lines, neither do the dotted lines. This is seen clearly in Fig. 4, which magnifies the lower center portion of Fig. 3. One feature that can be recognized

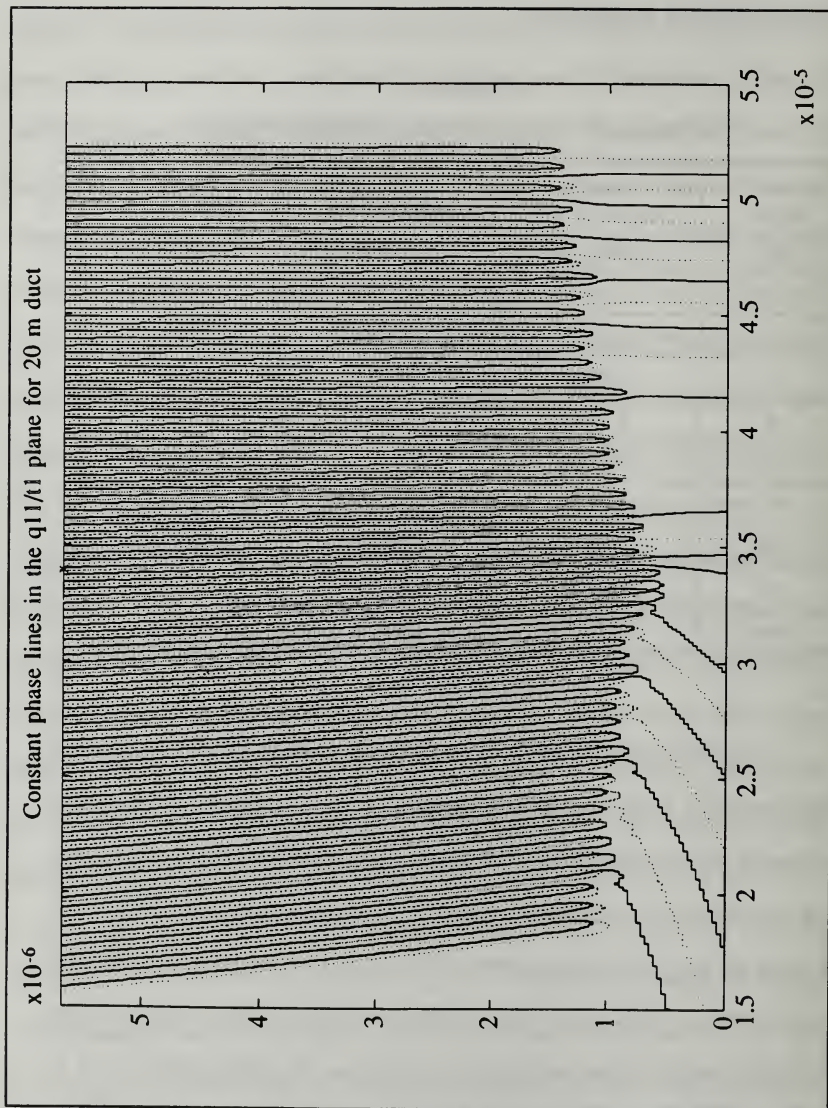


Figure 3. Constant phase lines in the  $q_1/t_1$  plane (20 m duct).

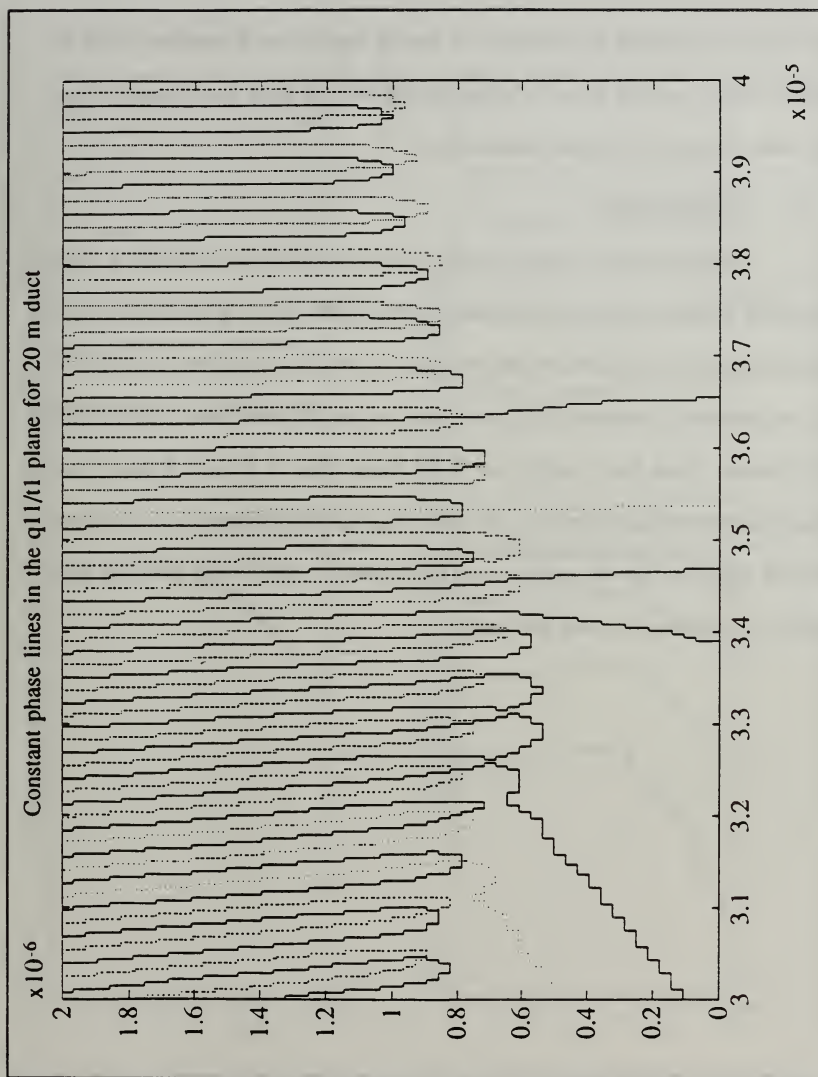


Figure 4. Magnified lower center portion of Fig. 3 showing no intersection of phase lines of the same type.



immediately in all the plots in Appendix D is that the starting real  $q$  coordinate given by Eq. (10), which is marked by an "x" along the top edge of each plot, correlates very closely with the mode of minimum attenuation.

## 2. Upward Tracking

One mode of low attenuation rate is missing from Fig. 2 compared to those found in Ref. 2. Several of them are also missing from those cases of greater duct heights plotted in Appendix D. It is evident that tracking the constant phase lines from the real  $q_{11}/t_1$  axis upwards is necessary. For the 10 meter and the 20 meter ducts, Fig. 5 shows several constant phase lines starting out of the lower limit of the search region and returning to the lower-half complex  $q_{11}/t_1$  plane. Fig. 6 shows the presence of such lines for the 30 meter and the 40 meter ducts. These constant phase lines have not been observed in those cases of lower duct heights.

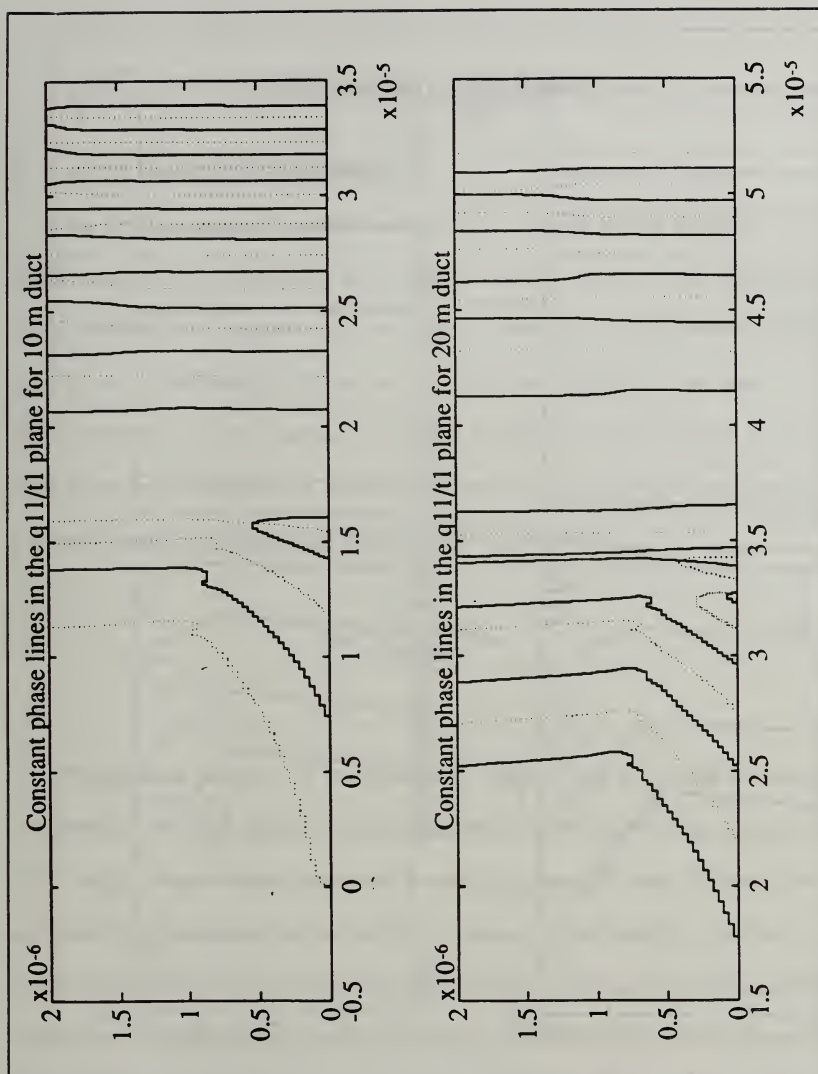


Figure 5. Upward going constant phase lines in the  $q_{11}/t_1$  plane for the 10 meter (top) and 20 meter (bottom) ducts.

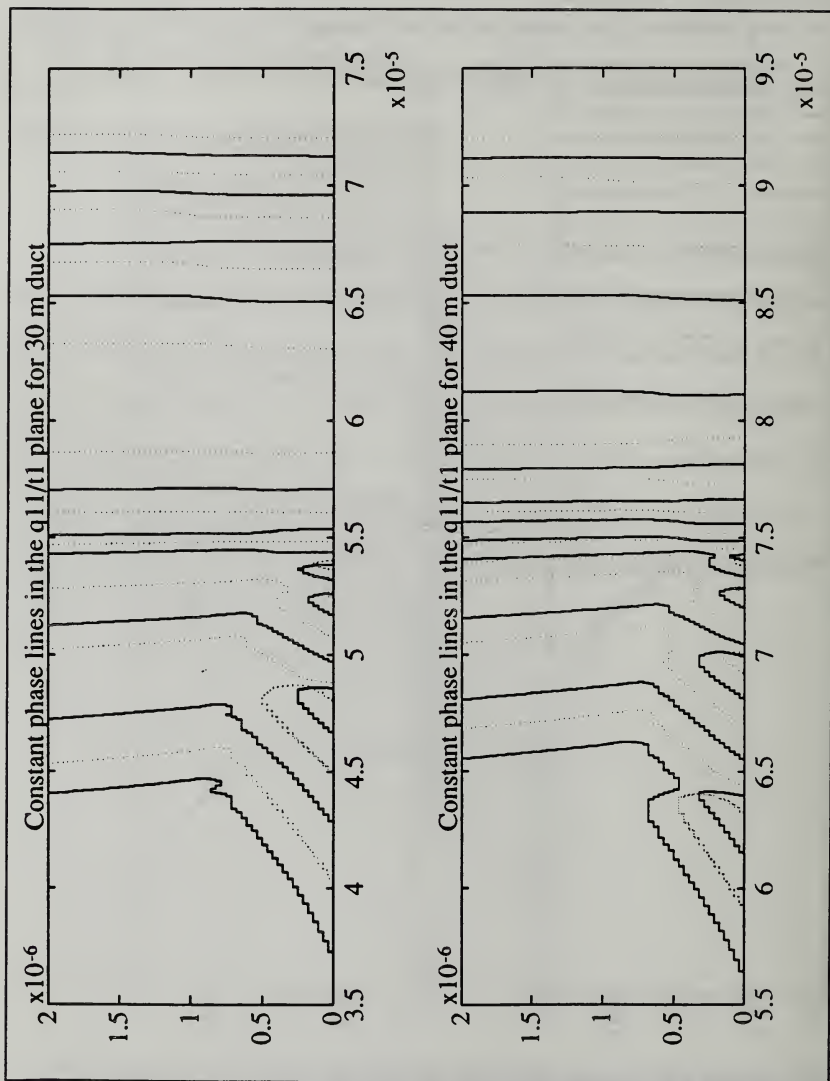


Figure 6. Upward going constant phase lines in the  $q_{11}/t_1$  plane for the 30 meter (top) and 40 meter (bottom) ducts.



### III. ANALYSIS AND CONCLUSIONS

#### A. MODE SEARCH PARAMETERS

The implementation of a mode search procedure requires several parameters. The search region has to be defined first. In M-Layer, the desired maximum range attenuation rate of the modes which support wave propagation is treated as an input parameter called  $a_{\text{loss}}$ , given conventionally in dB per km. This parameter determines the region over which the modes are to be searched as explained in Chapter I. In the complex  $q$  plane, under the assumption that both  $m_1$  and  $\beta/k$  of interest are close to unity, the search region is bounded from above by the FORTRAN variable  $q_{\text{top}}$  given by

$$q_{\text{top}} = \frac{10^{-4} t_1}{k \times \log_{10} e} a_{\text{loss}}. \quad (12)$$

The location at which to start the mode search,  $q_{\text{test}}$ , is another parameter determined by M-Layer. Based on optical considerations, the M-deficiency,  $d_{\text{mmin}}$  of Fig. 1, which is the amount of decrease of the modified refractivity from its value on the sea surface to its minimum value in the air, is a measure of the capability of the duct to trap electro-magnetic waves. As explained also in Chapter I, this quantity determines the location for the program to start searching for modes. The validity of the optical argument and the usefulness of Eq. (10) have been proved by this work, as pointed out in Chapter

## II.

To search for zeros of the mode function, M-Layer first covers the search region with identical mesh squares. It then follows the lines of the type  $\text{Im}\{D(q)\} = 0$  through each mesh square, checking for indications that a curve  $\text{Re}\{D(q)\} = 0$  is entering the same mesh so that an intersection is possible. The term "mesh size" will denote the size of the edges of the mesh squares. It is the size of the step taken by the program to advance through the search region. It also determines the initial resolution of the location of a mode. The choice of the mesh size should strike a balance between the desire for a speedy completion of the search process and the requirement in mode locating accuracy. As reported in Ref. 2, for all the evaporation ducts considered, the choice of a mesh size equivalent to an attenuation rate of 1/32 dB per km appears to be optimal, that is, all modes can be found for all cases investigated in Ref. 2 without experiencing extraordinarily long computation time. Consider this mesh size as the default and call it  $q_d$  in the complex  $q$  plane. Under the same assumption for deducing Eq. (12), the value of  $q_d/t_1$  at 9.6 GHz equals  $3.58 \times 10^{-8}$ . Figure 7 shows the separation between two adjacent constant phase lines of the type  $\text{Im}\{D(q)\} = 0$ , indicated in the figure as solid lines, along the top edge of the search region for the 20 meter duct. The minimum of these separations in terms of  $q_{11}/t_1$  is about  $2.8 \times 10^{-7}$ , which corresponds to a spacing of a little less than eight mesh squares apart. The minimum separation between adjacent  $\text{Im}\{D(q)\} = 0$  and  $\text{Re}\{D(q)\} = 0$  lines is thus about four meshes. Constant phase line separations for all evaporation ducts considered are included in Appendix E. Note that the minimum separation is almost constant for ducts higher than 20 meters. It increases

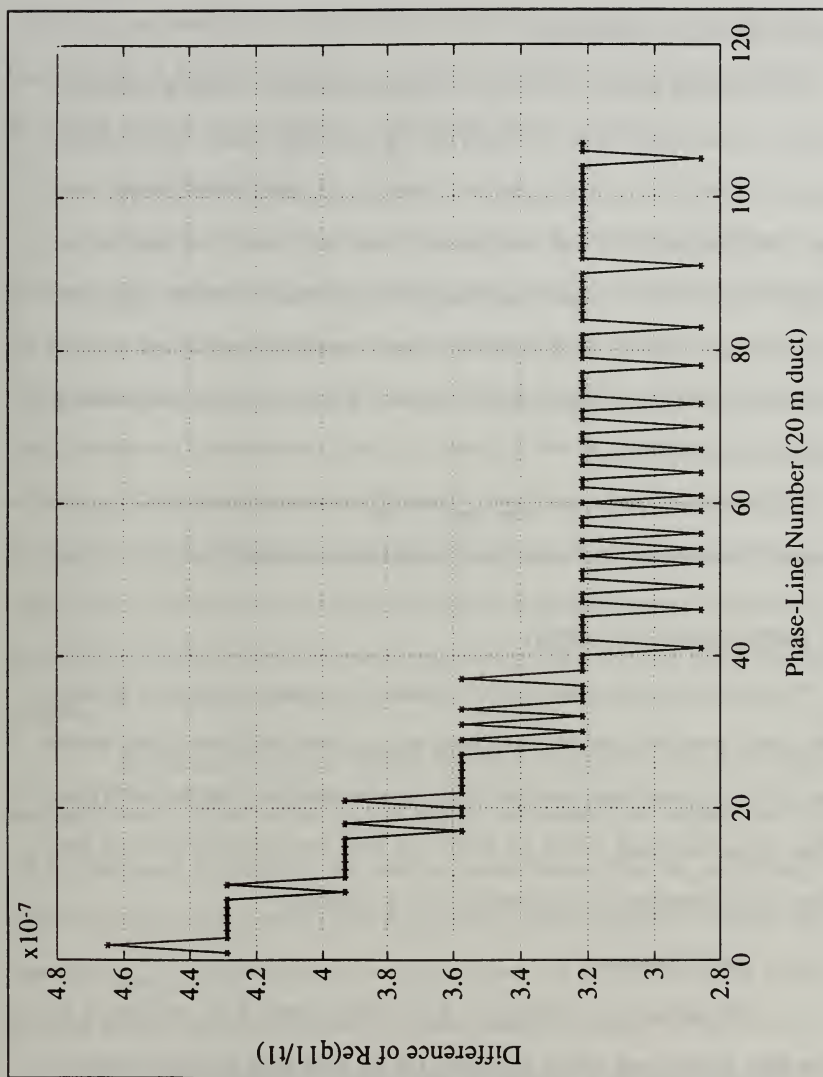


Figure 7. Separation of  $\text{Im}\{D(q)\} = 0$  lines along the top edge of the search region (20 m duct).

slightly as duct height is decreased.

As the program follows an  $\text{Im}\{D(q)\} = 0$  line into the search region, a neighboring  $\text{Re}\{D(q)\} = 0$  line moves closer and enters into the same mesh square. This causes the program to invoke the root finding routine to determine the possible locations of zeros of the mode function within this mesh square. If the mesh size is too large and the  $\text{Re}\{D(q)\} = 0$  line enters the mesh square long before the actual intersection takes place, the root finding routine will be prematurely invoked many times and the probability of producing false modes is increased. This explains why a larger mesh size sometimes will increase the execution time.

Given these three parameters  $q_{\text{top}}$ ,  $q_{\text{test}}$ , and  $q_d$ , a mode search strategy which does without the "contour rectangles" is proposed. It should improve the efficiency of M-Layer.

## B. MODE SEARCH STRATEGY

From the constant phase line plots of Appendix D, a strategy to search for the mode can be drawn: move along the top edge starting at  $q_{\text{test}}$ . Search first toward either the left or the right, then reverse course to search along the other direction. After the search along the top edge is completed, search the lower edge from one end to the other. In what follows, the implementation of this strategy will be discussed.

### 1. Track Termination

The tracking of an  $\text{Im}\{D(q)\} = 0$  line naturally ends if the top edge or the bottom edge of the search region is reached. On the other hand, the search region is unbounded to the right and left of  $q_{\text{test}}$ . It is convenient to retain the feature in the

original program to set a limit on the number of steps allowed to follow a constant phase line. From Fig. 3, this limit can be set to 2.5 times the number of mesh squares between the vertical limits of the search region. This number equals  $2.5 \times 32 \times a_{\text{loss}}$ .

## 2. Search Termination

M-Layer has to determine that no more modes within the search region is to be found and to terminate the search for modes. When searching along the top edge of the search region for the constant phase lines  $\text{Im}\{D(q)\} = 0$ , the separation between the real parts of the mode eigenvalues is of interest. Figure 8 shows the separation in the real part of neighboring  $q$ -eigenvalues scaled by  $t_1$ , plotted against their locations  $q_m/t_1$  along the real  $q_{11}/t_1$  axis for the case of the 20 m duct. Similar plots for all duct heights are grouped in Appendix F. Excluding the lowest point which involves the mode obtained via searching along the lower edge, the separation between neighboring modes is erratic with an upward trend away from the center of the figure, which is close to the search starting position.

The increase in distance between two modes towards the end of the range searched makes it difficult to implement an adaptive mechanism to terminate the search. On the other hand, Fig. 3 shows that almost all phase lines entering the search region from the top that contain a mode within this region are bunched together. Therefore, the parameter  $n_{\text{stop}}$ , set equal to four and may be adjusted, can be used to stop the search along the top edge when four consecutive constant phase lines tracked turn up no mode.

The search along the real  $q$  axis can be confined to within the end points of the search along the top edge.

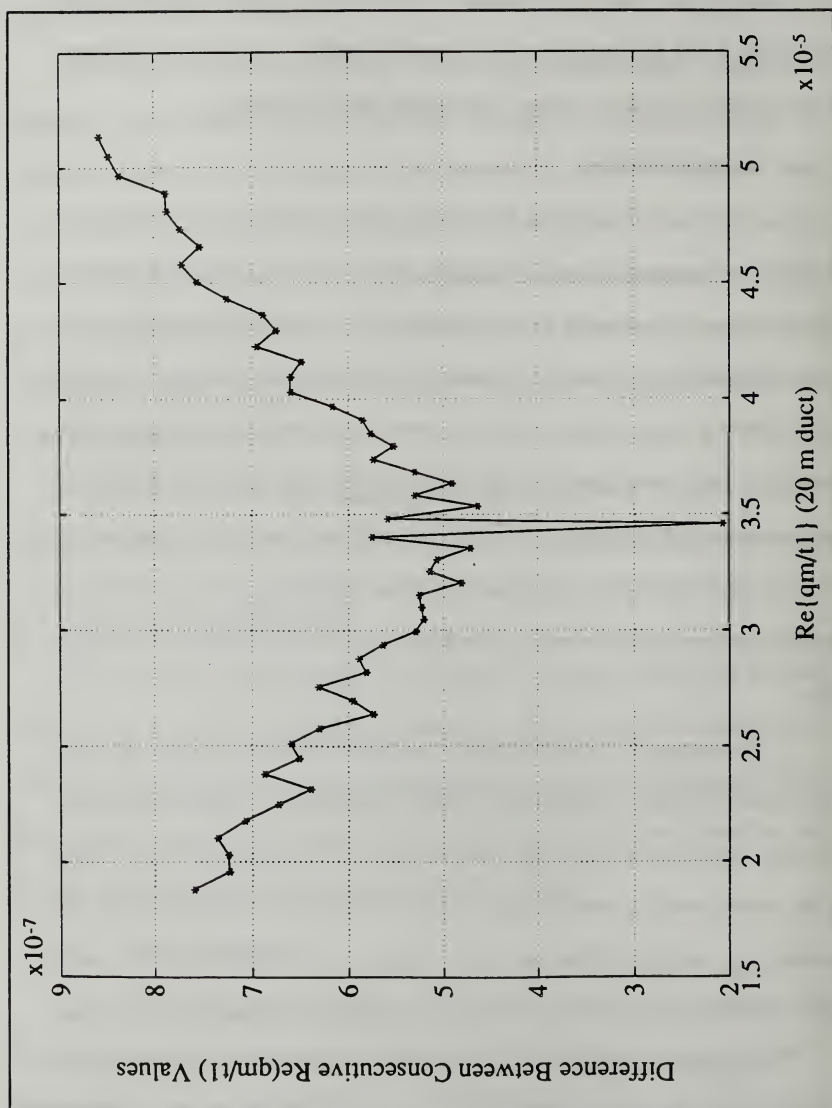


Figure 8. Difference between consecutive  $Re(q_m/t_l)$  values (20 m duct).



### 3. Track Duplication Avoidance

When the program searches step by step along the top or bottom edges for sign changes in  $\text{Im}\{D(q)\}$  to start tracking the constant phase line, the exit of a constant phase line from a previous track will be encountered. Entering into the search region at such a location will simply retrace a constant phase line which has already been examined for the existence of a mode. Thus, the exit locations of the constant phase lines must be recorded and checked whenever a sign change in  $\text{Im}\{D(q)\}$  is found before deciding to follow the constant phase line into the search region. Along the top edge, a record of four updated most recent exit locations from the top edge should be adequate. The locations of exits from the bottom should be kept for use during the search along the lower edge of the search region. For this record, a dimension of 256 should be adequate for the current cases. But this dimension should be adjusted if other types of ducts are studied. A record of four of the most recent exit locations out of the lower edge should also be kept and checked to avoid duplicate tracking of the constant phase lines.

## APPENDIX A: MODE LOCATIONS IN THE COMPLEX $q_{11}/t_1$ PLANE

This appendix contains figures of mode locations of evaporation ducts of 2, 4, 6, 8, 10, 20, 30, and 40 m heights plotted in the complex  $q_{11}/t_1$  plane for easy comparison.



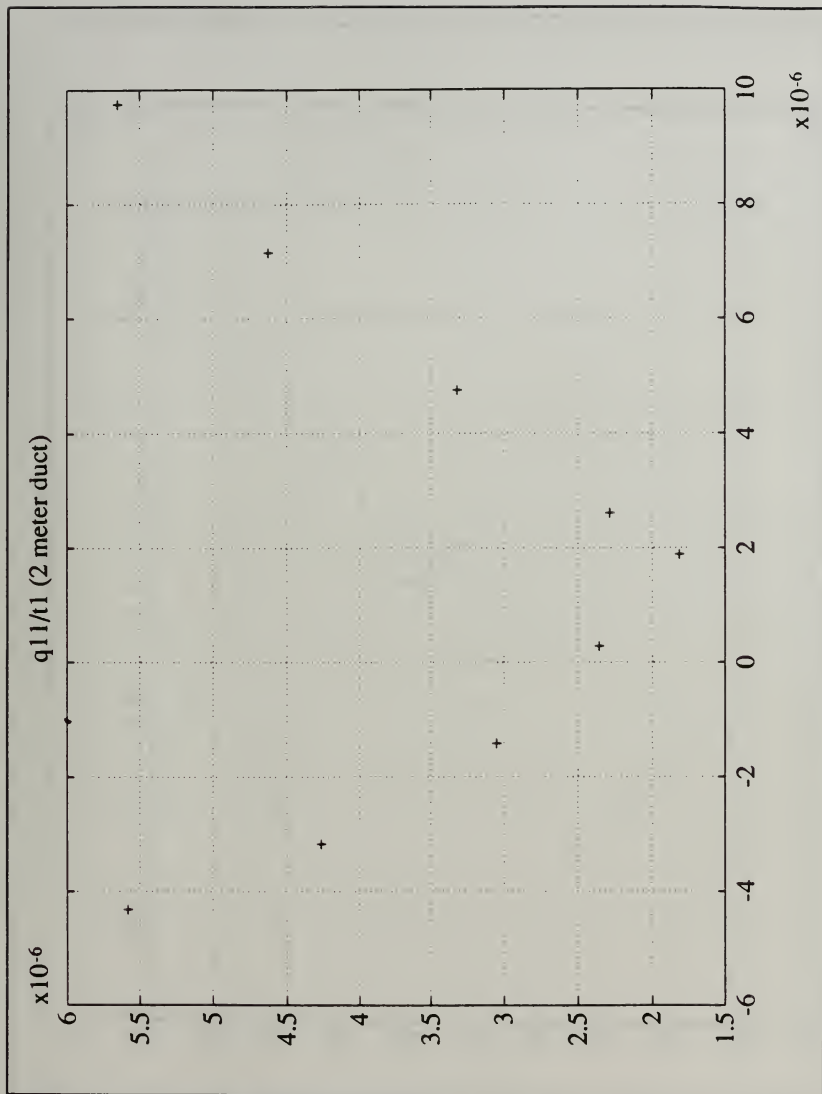


Figure A.1  $q_{11}/t_1$  mode locations (2 m duct).

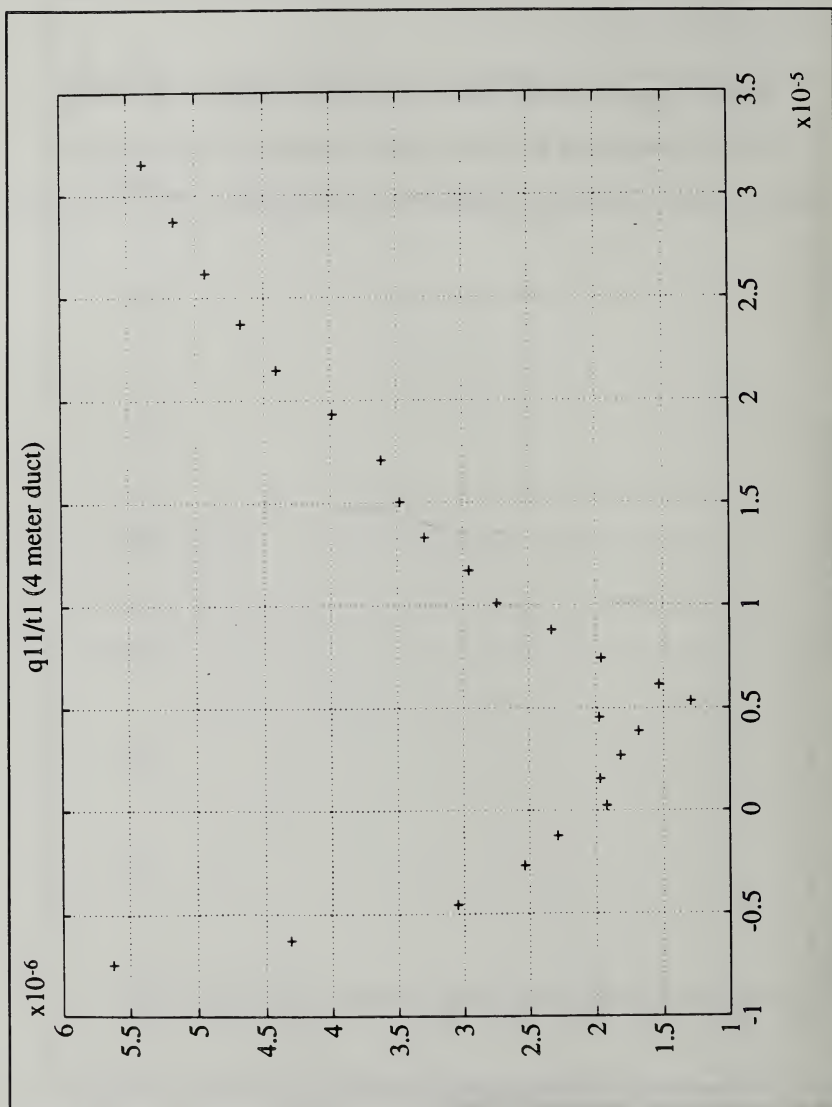


Figure A.2  $q_{11}/t_1$  mode locations (4 m duct).

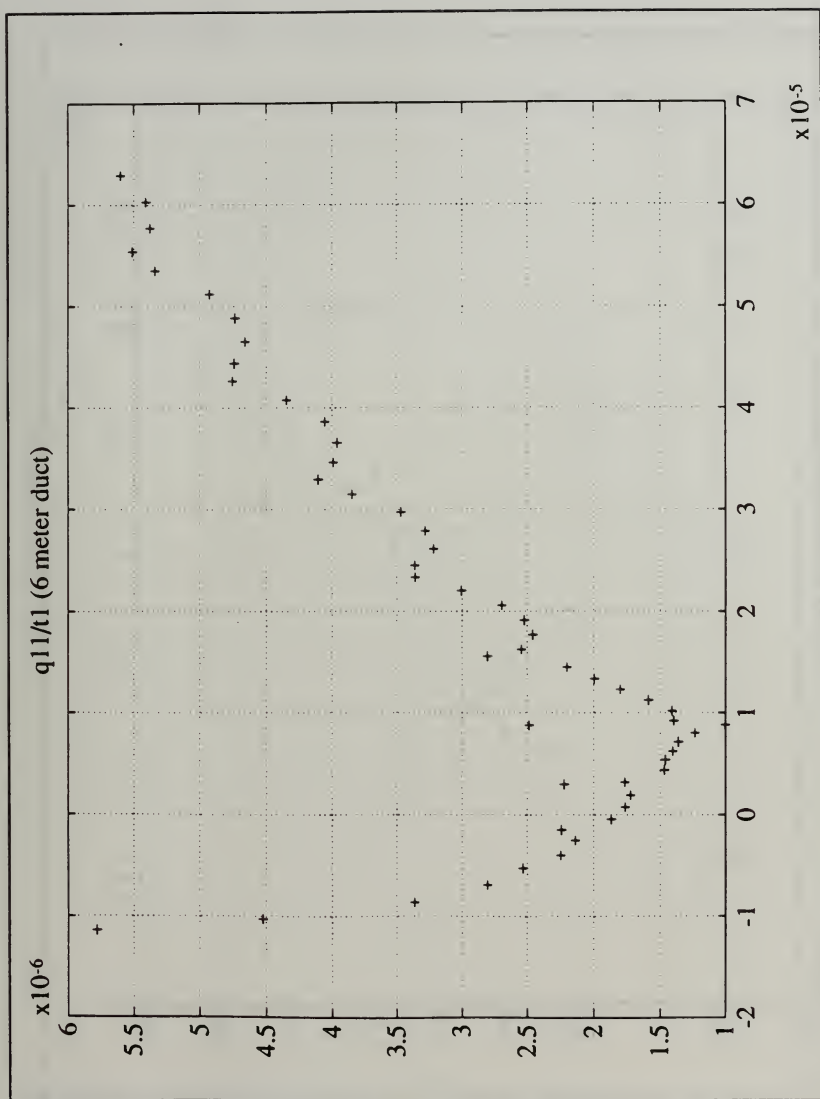


Figure A.3  $q_{11}/t_1$  mode locations (6 m duct).

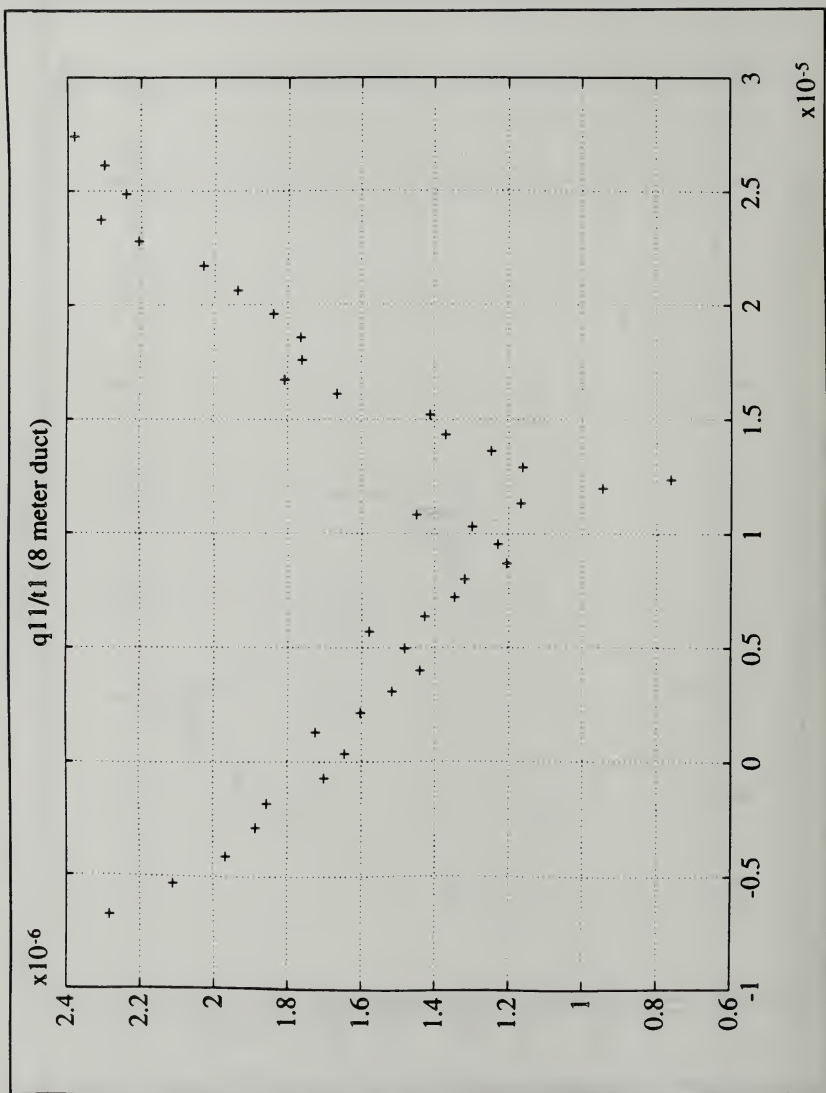


Figure A.4  $q_{11}/t_1$  mode locations (8 m duct).

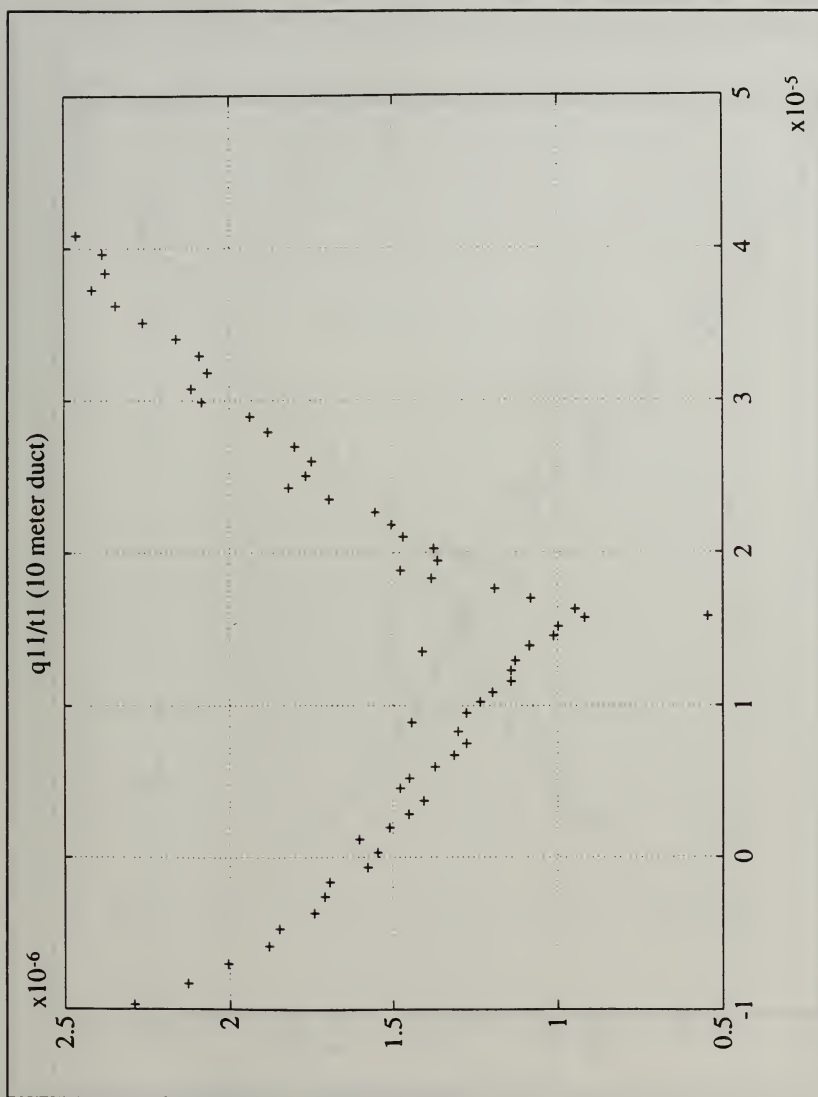


Figure A.5  $q_{11}/t_1$  mode locations (10 m duct).

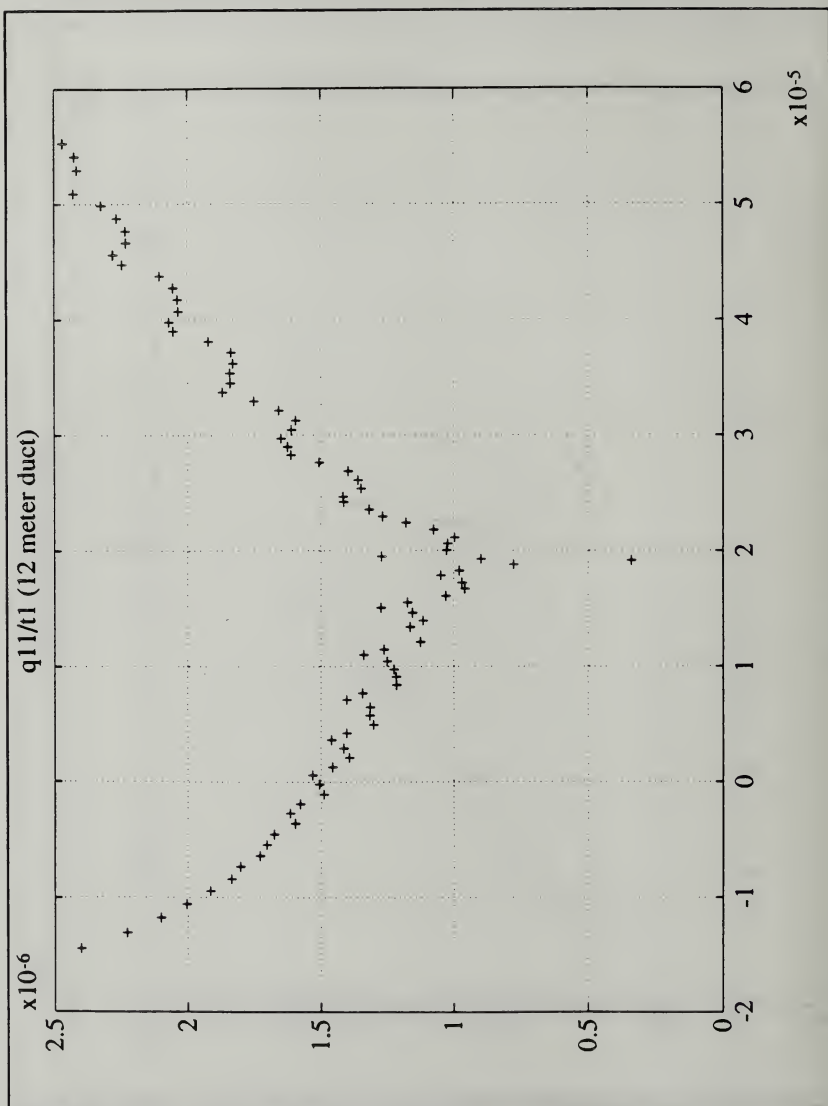


Figure A.6  $q_{11}/t_1$  mode locations (12 m duct).

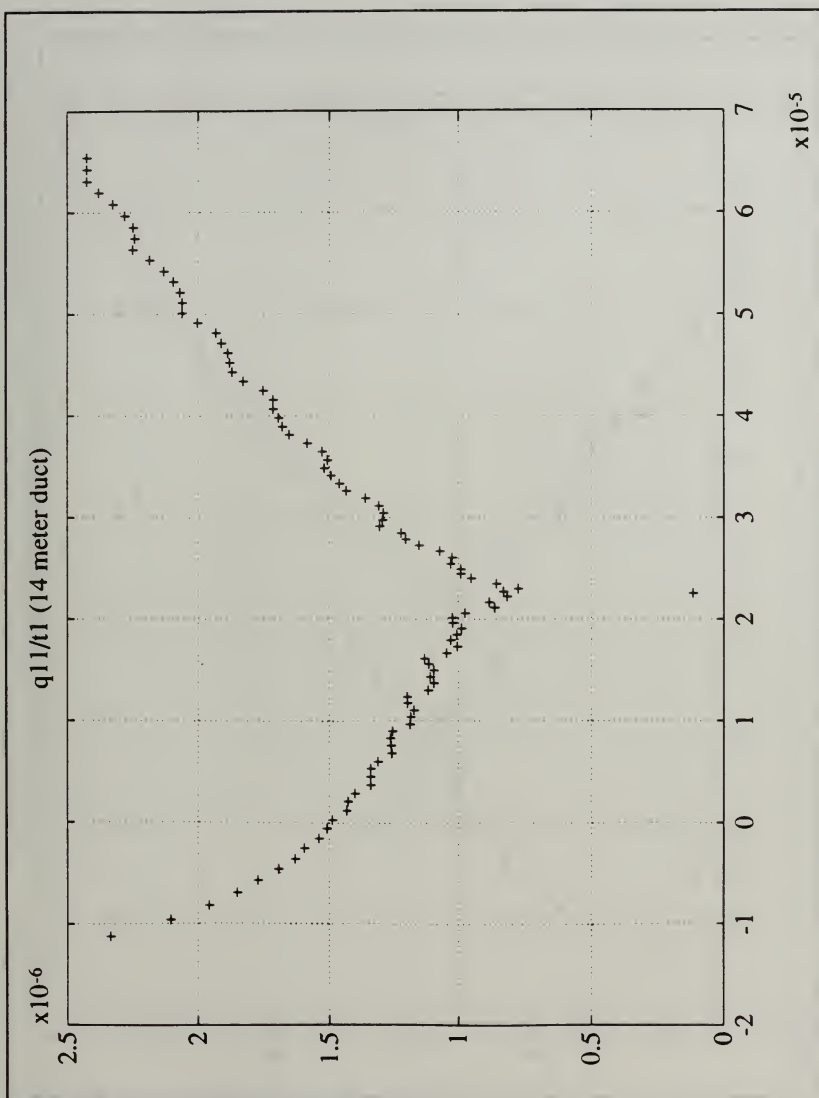


Figure A.7  $q_{11}/t_1$  mode locations (14 m duct).



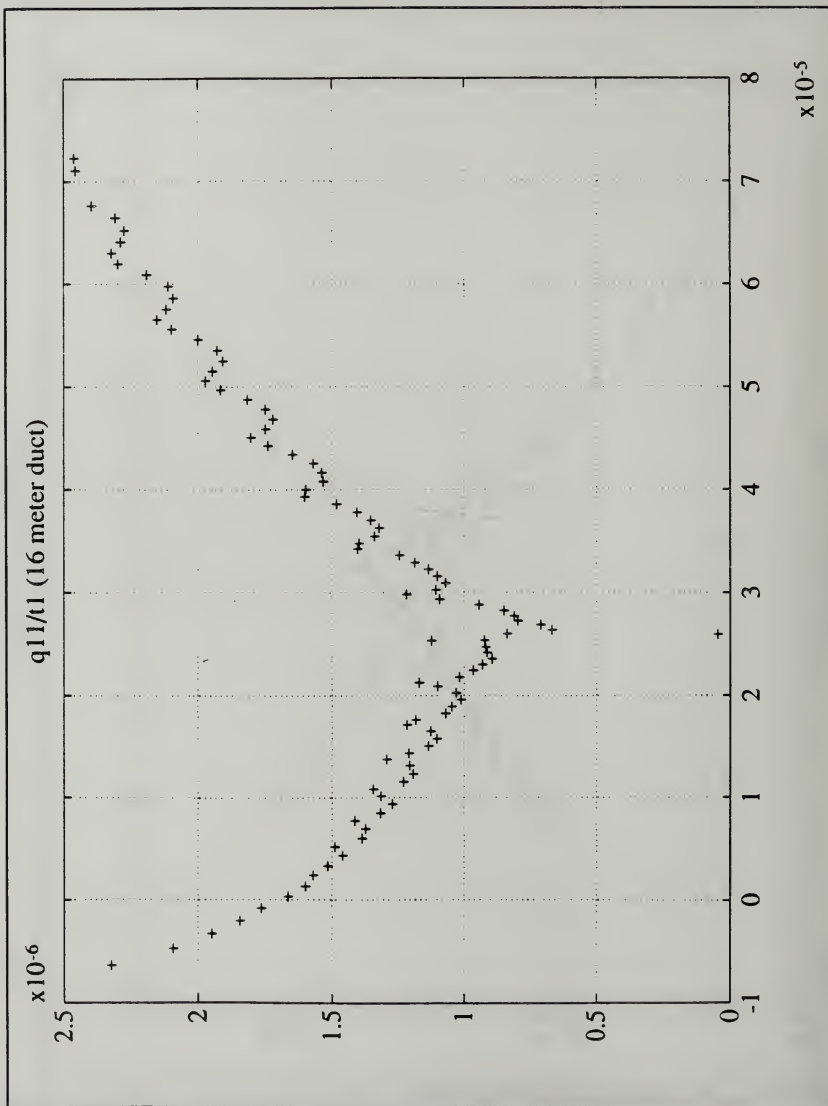


Figure A.8  $q_{11}/t_1$  mode locations (16 m duct).

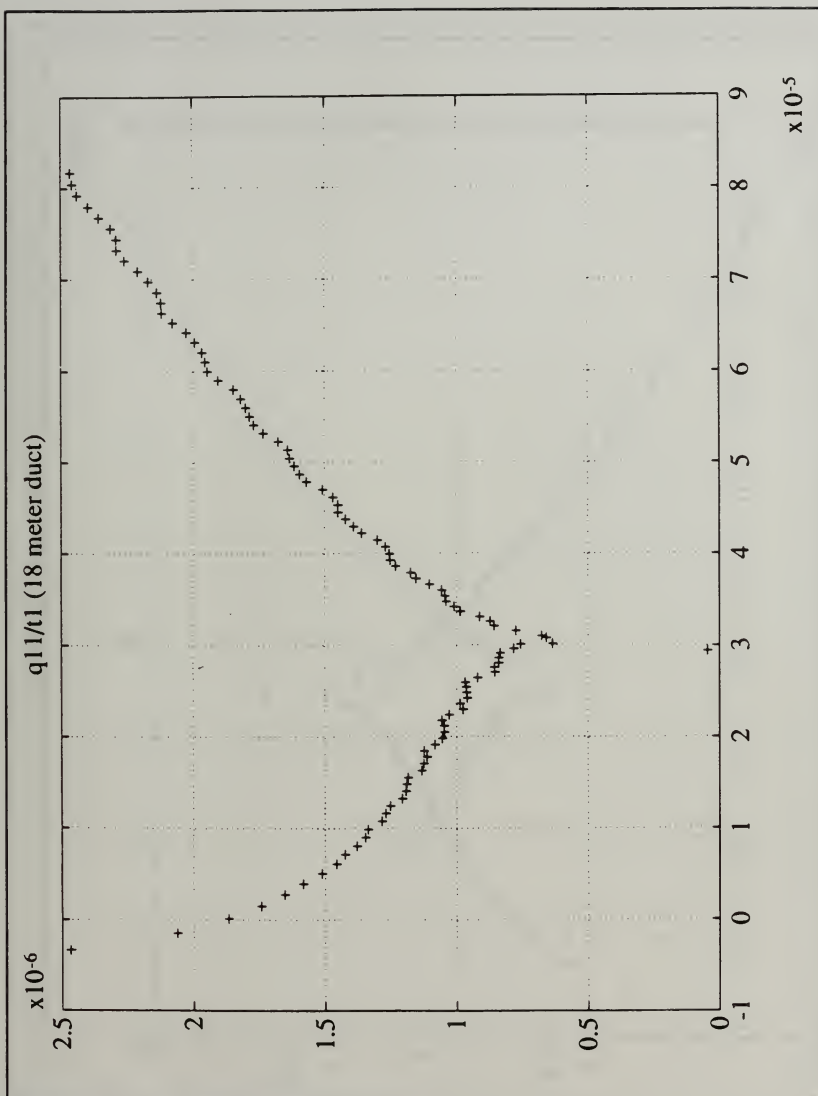


Figure A.9  $q_{11}/t_1$  mode locations (18 m duct).

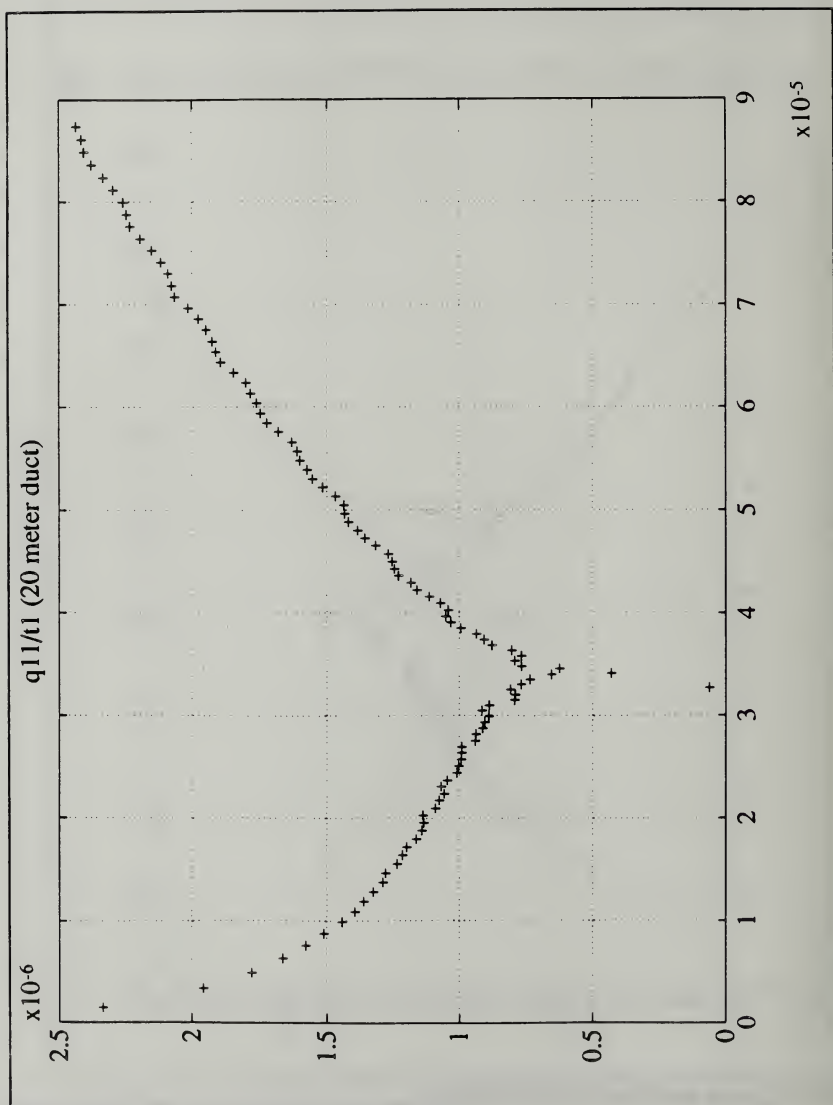


Figure A.10  $q_{11}/t_1$  mode locations (20 m duct).

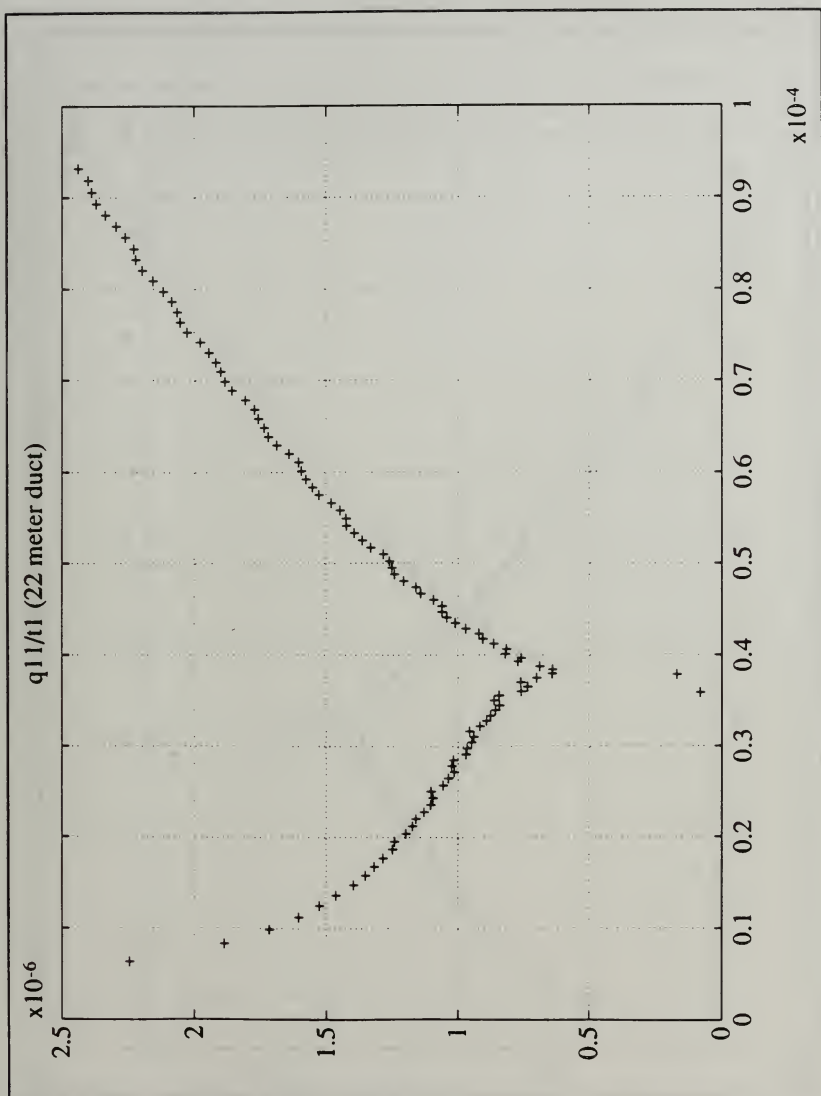


Figure A.11  $q_{11}/t_1$  mode locations (22 m duct).

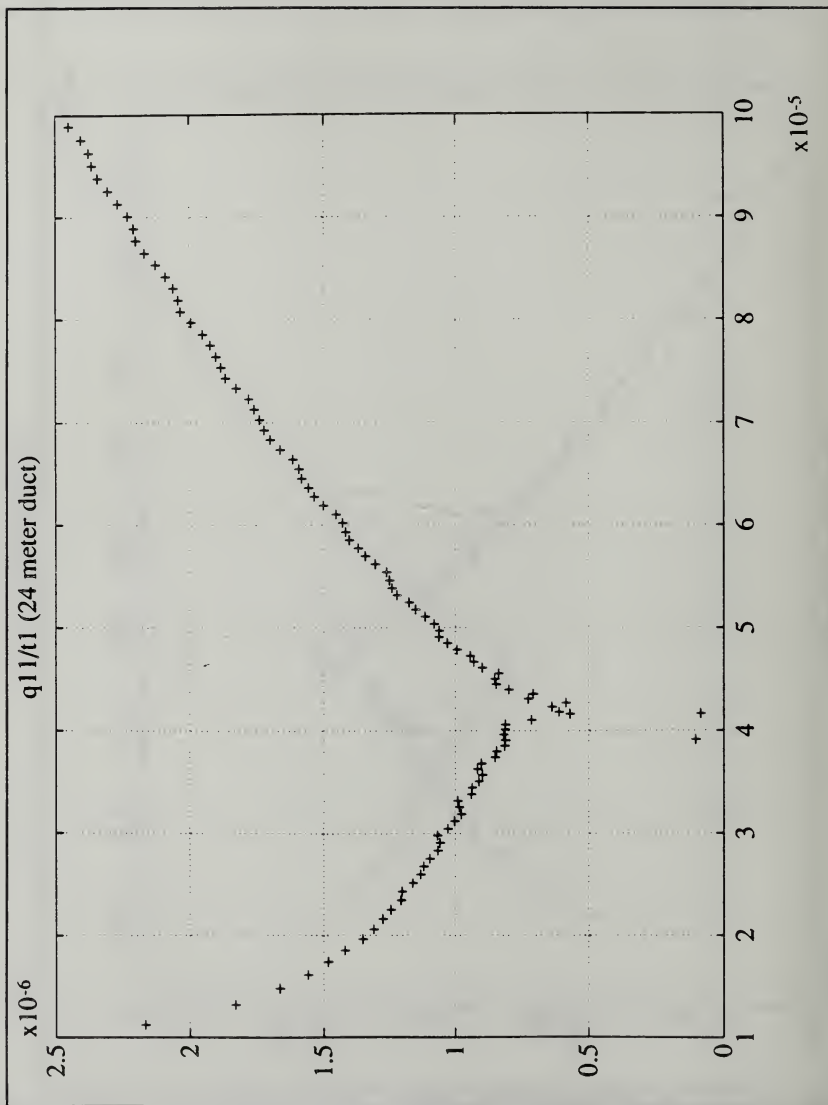


Figure A.12  $q_{11}/t_1$  mode locations (24 m duct).

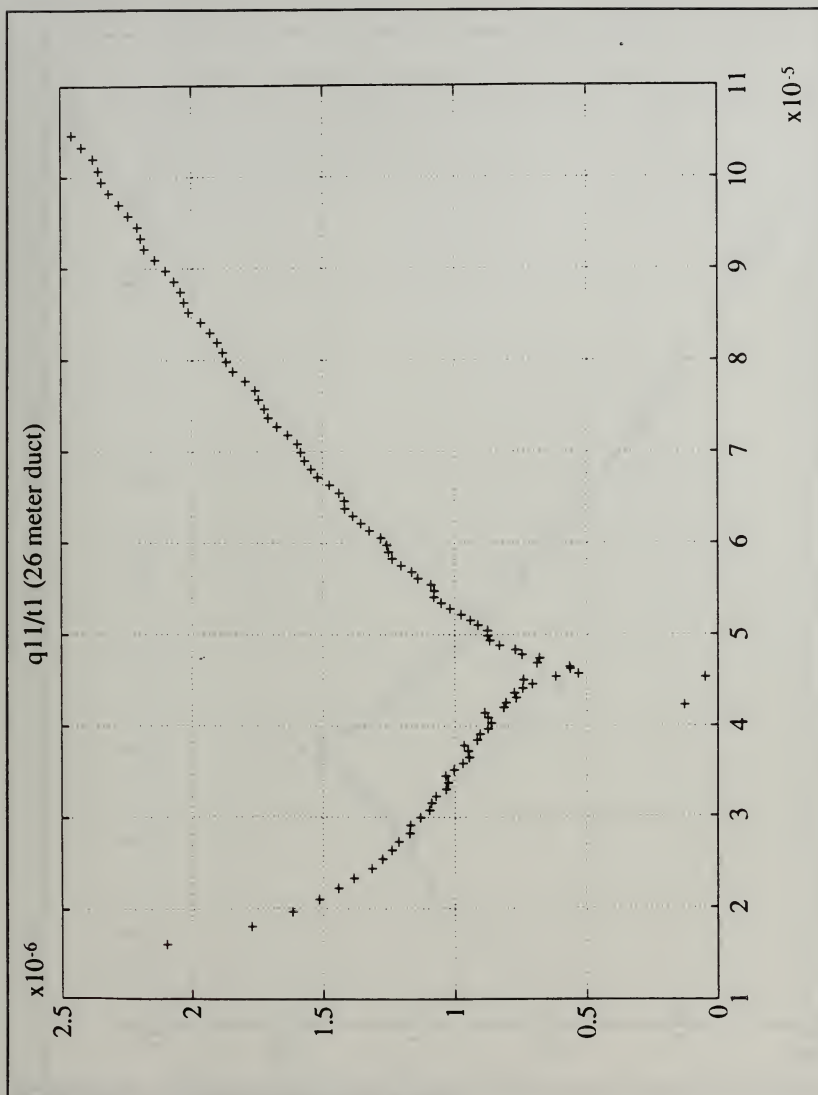


Figure A.13  $q_{11}/t_1$  mode locations (26 m duct).

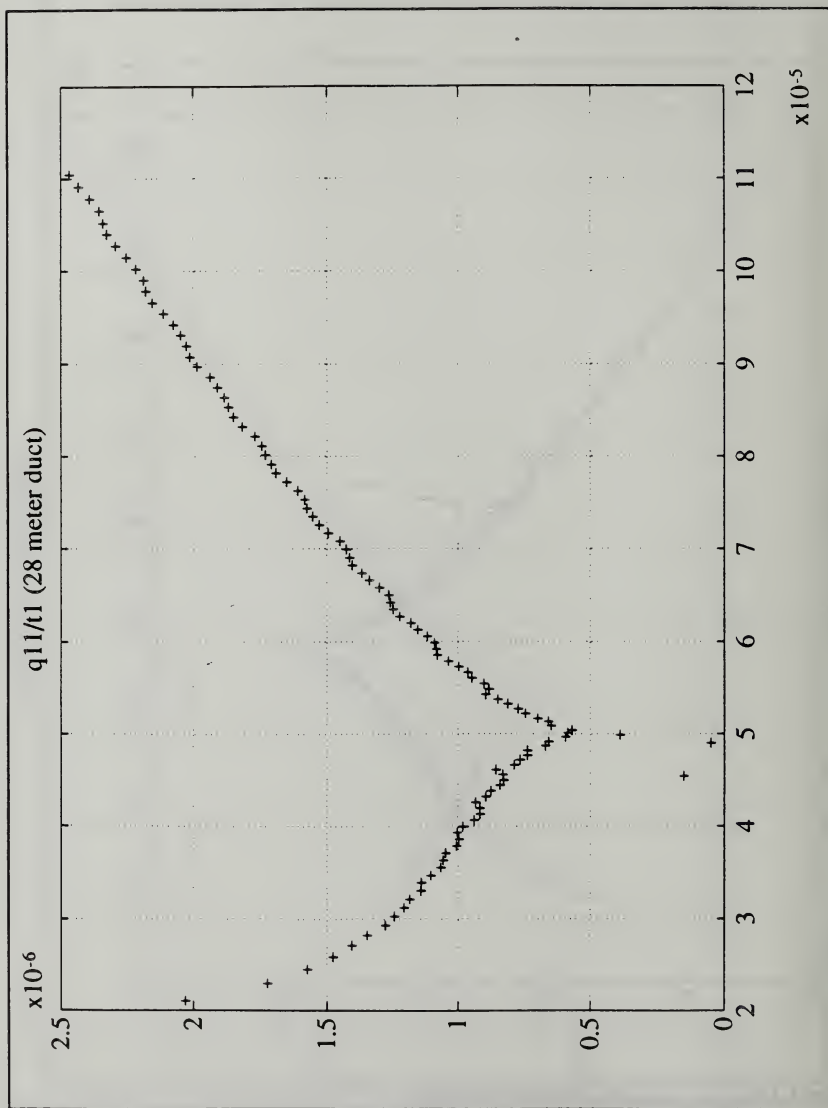


Figure A.14  $q_{11}/t_1$  mode locations (28 m duct).



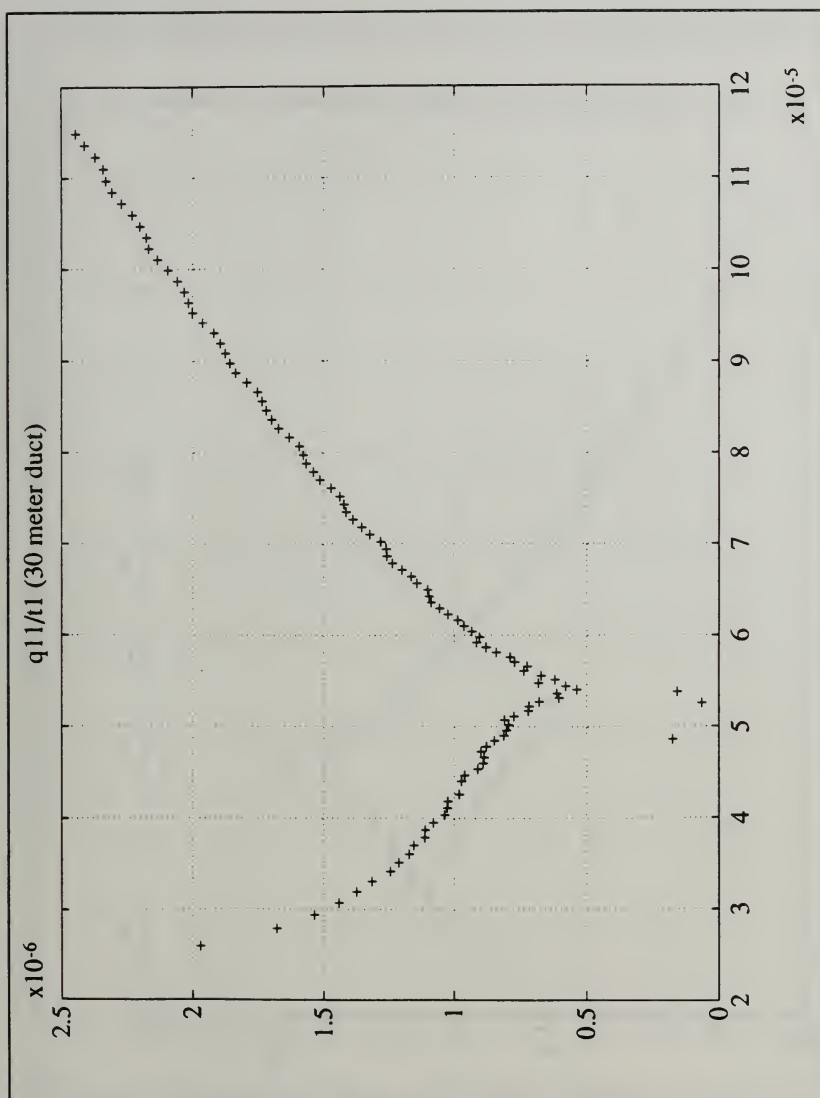


Figure A.15  $q_{11}/t_1$  mode locations (30 m duct).

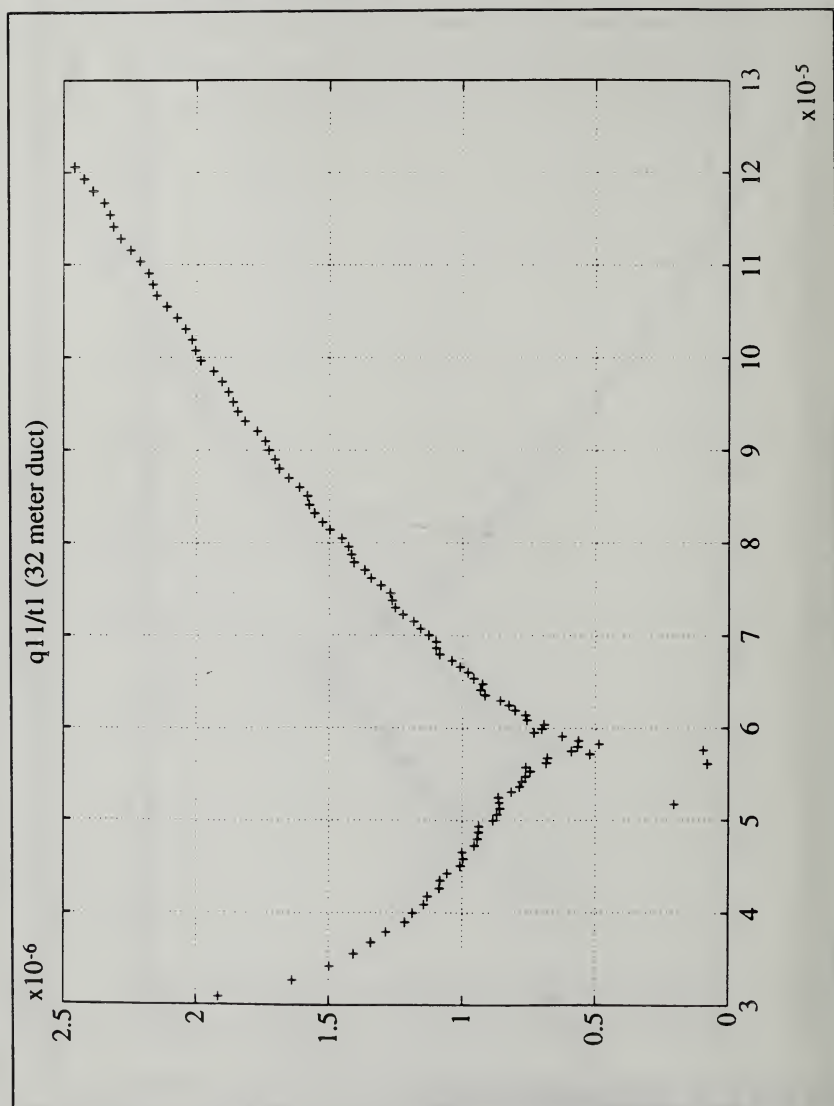


Figure A.16  $q_{11}/t_1$  mode locations (32 m duct).

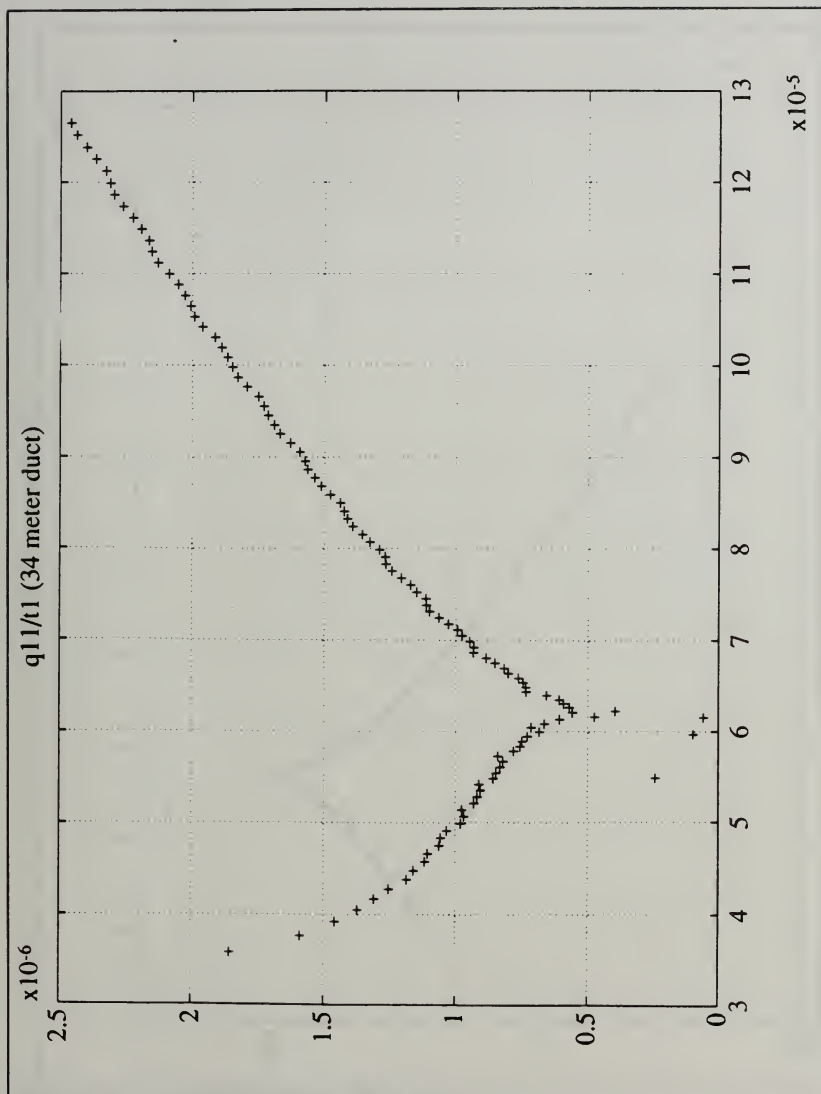


Figure A.17  $q_{11}/t_1$  mode locations (34 m duct).

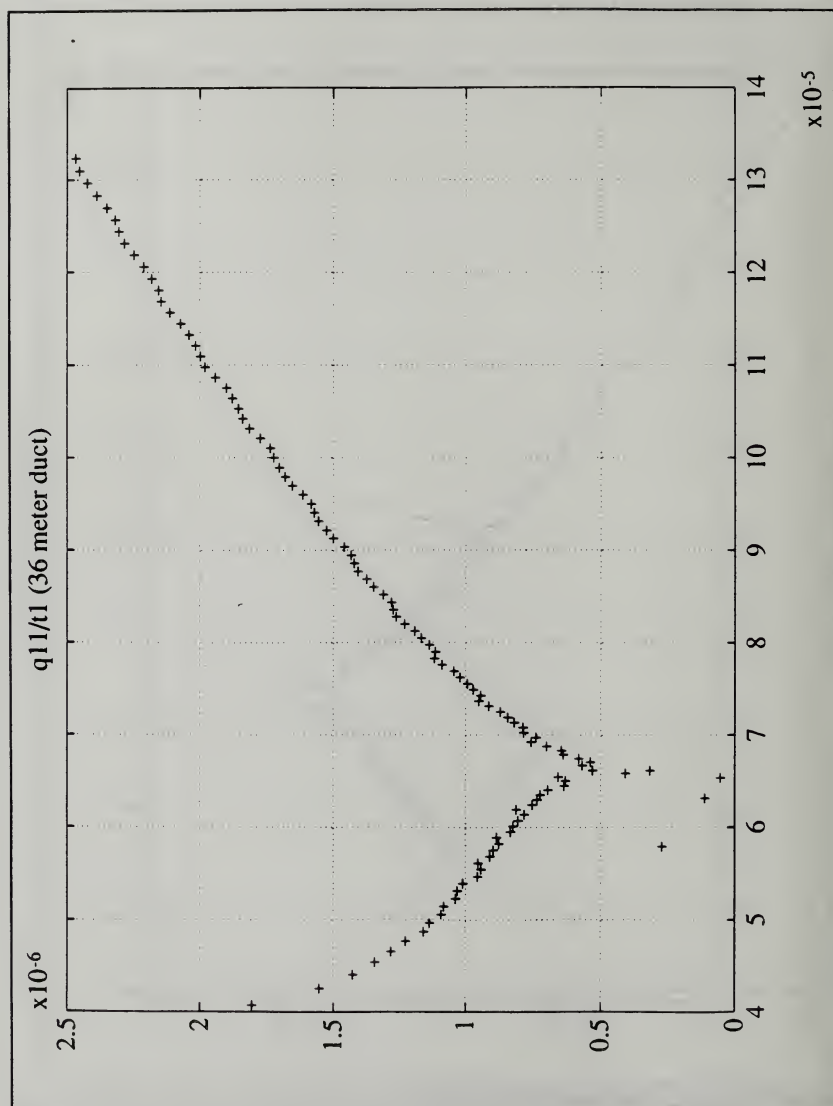


Figure A.18  $q_{11}/t_1$  mode locations (36 m duct).

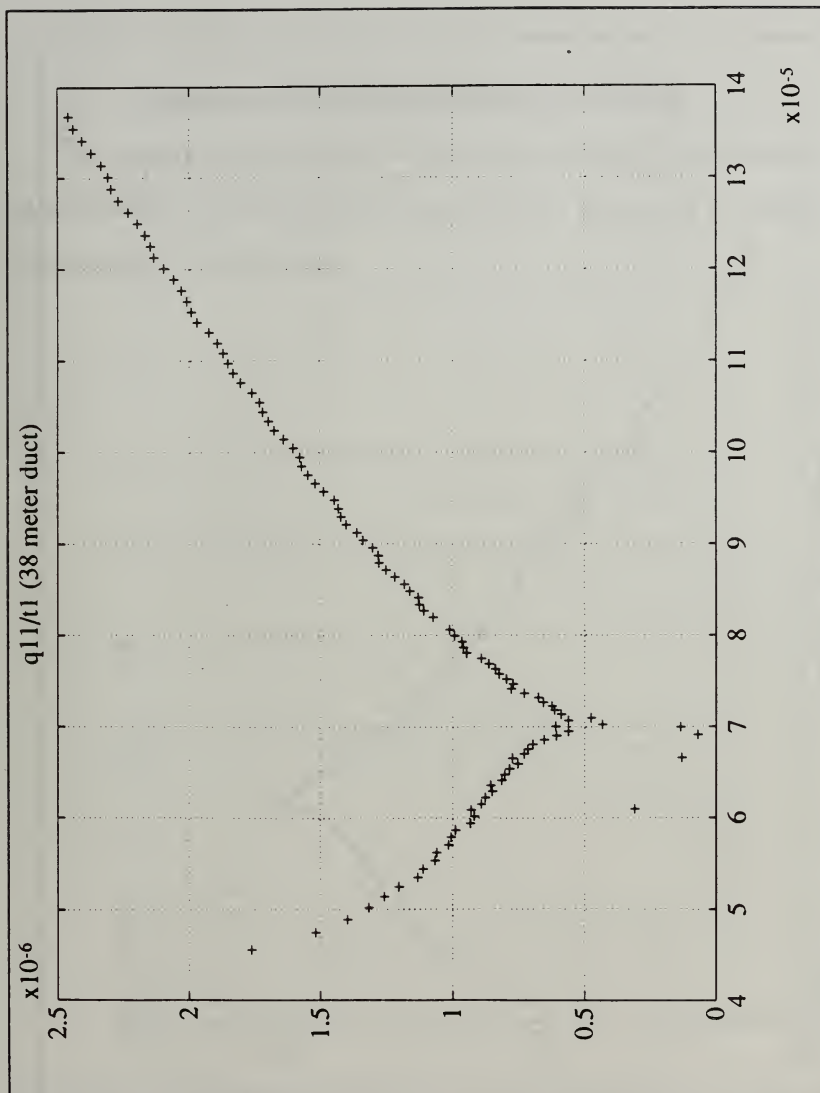


Figure A.19  $q_{11}/t_1$  mode locations (38 m duct).

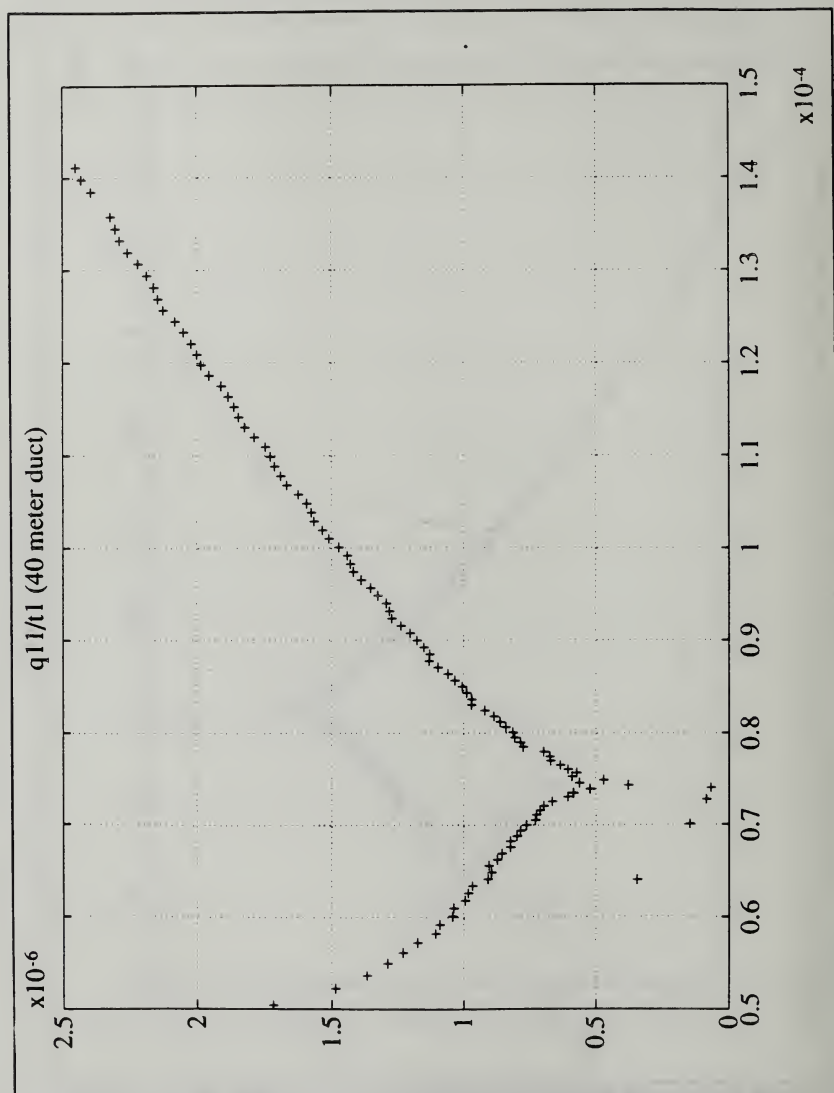


Figure A.20  $q_{11}/t_1$  mode locations (40 m duct).

## APPENDIX B: SUBROUTINE FNDMOD AND FZEROX

This appendix contains the listing of the subroutines FNDMOD and FZEROX, modified from the NPS version of the M-Layer FORTRAN code to track the constant phase-lines and to locate the modes.



```

Line# Source Line   Microsoft FORTRAN Optimizing Compiler Version 5.00
1      subroutine fndmod(aloss,dmmin,t1,dmesh,filem,nrmode,qeigen)
2
3      c purpose:
4      c   This subroutine sets up the areas in the complex q11-plane
5      c   to search for the zeroes of the modal function.
6      c
7      c inputs...
8      c   mxlayr - maximum number of layers allowed in refractivity
9      c   profile
10     c   nzlayr - actual number of layers in refractivity profile
11     c   aloss  - maximum attenuation rate (in db/km) of modes
12     c           to be found
13     c   dmmin  - minimum of zim(j)-zim(1)
14     c   t1     - koa123
15     c   dmesh  - initial mesh size divisor
16     c
17     c outputs...
18     c   qeigen - complex array containing the zeros of the modal
19     c           function
20     c   nrmode - actual number of modes found
21     c
22     c subroutines called...
23     c   fzerox
24     c   findfx
25     c common block areas...
26     c   com1
27     c*****
28     c
29     c   implicit double precision (a-h,o-z)
30     c   complex*16 ctemp,t1,qeigen,zeros,fx1,fx2
31     c   parameter(c20log=8.68588963806504d0,one=(1.d0,0.d0),
32     c   $         step0=1024.d0,step0h=step0/2.d0)
33     c   character*3 filem,kline
34     c   character*40 rfile
35     c
36     c*****
37     c   qeigen  - complex array containing all the zeros of the
38     c           modal function found
39     c   zeros   - complex array containing the zeros of the modal
40     c           function found in the current rectangular region
41     c           of the complex q11-plane
42     c
43     c*****
44     c   use include file for parameters of
45     c           mxlayr max # layers
46     c           mxmode max # modes
47     c
48     $include: 'mlaparm.inc'
      ***** Begin listing of: mlaparm.inc

```

```

1 c
2 c      include file to define the
3 c          maximum # of layers (mxlayr)
4 c          maximum # of modes (mxmode)
5 c
6 c      parameter (mxlayr=35 )
7 c      parameter (mxmode=127 )
8 c      ***** End listing of: mlaparm.inc
49
50      dimension qeigen(mxmode),zeros(2*mxmode+1)
51 c*****
52      common /com1/waveno
53 c
54 c*****
55 c      r1 - value of mode search on the real part of q11 at the
56 c          left edge in tmesh units.
57 c      r2 - value of mode search on the real part of q11 at the
58 c          right edge in tmesh units.
59 c      bot - value of the imaginary part of q11 at the bottom
60 c          edge (this is set to 0).
61 c      t0 - value of the imaginary part of q11 at the top edge
62 c          in tmesh units.
63 c      step - size of search areas.
64 c*****
65 c
66 c
67 c -----
68 c          start of executable statements
69 c -----
70 c*****
71 c      set up search areas for finding modes and solve for modes,
72 c      calculate approximate value for re(q11) where modes start
73 c      occurring
74 c*****
75 c
76 c      nrmode=0
77 c
78 c      recons=dreal(t1)
79 c      rstart=-2.0d-6*dmmin
80 c      qtest=rstart*recons
81
82 c      ttop1=(2.0d-3/(waveno*c20log))*recons
83 c      ttop=aloss*ttop1
84 c      tmesh=ttop1/dmesh
85 c      if(tmesh .gt. 0.1d0) tmesh=1.0d-1
86 c      if(tmesh .gt. 1.0d-3) then
87 c          tol=1.0d-4
88 c      else
89 c          tol=tmesh*0.1d0
90 c      end if

```

```

91 c
92 c*****
93     write(*,1002)
94     write(16,1002)
95 c
96     write(*,1003) tmesh,tol
97     write(16,1003) tmesh,tol
98 c
99     t0=dnint((ttop/tmesh)+1.d0
100     bot=0.d0
101 c*****
102 c
103     r1=dnint(qtest/tmesh)-step0h
104     r1=r1
105     rr=r1+step0
106     call findfx(r1,t0,fx1,x1,y1,tmesh)
107     i1=int(r1)
108     in=int(step0)+int(r1)
109     nline=0
110 50  continue
111     do 100 nn=i1,in
112         r2=r1+1.d0
113         call findfx(r2,t0,fx2,x2,y2,tmesh)
114         if (y1*y2 .lt. 0.d0) then
115             r=r1*tmesh
116             write (*,5555) r
117 c         write (16,5555) r
118 5555     format (/5x,'r= ',d28.16)
119             go to 400
120         endif
121         r1=r2
122         fx1=fx2
123         x1=x2
124         y1=y2
125 100 continue
126     return
127 c
128 400  continue
129     nrold=nrmode
130     nline=nline+1
131     nc100=int(nline/100)
132     nc10=int((nline-nc100*100)/10)
133     nc1=nline-nc100*100-nc10*10
134     kline=char(48+nc100)//char(48+nc10)//char(48+nc1)
135     rfile='e:\ans5v'//filem//kline//'.dat'
136 c*****
137     open (unit=25,file=rfile,status='unknown')
138
139     call fzerox(t0,r1,r11,fx1,x1,y1,fx2,x2,y2,zeros,nrold,nmew,
140     $         tmesh)

```

```

141      close (25)
142 c*****
143 c
144      nrmode=nrnew
145      new0=nrmode-nrold
146 c
147 c*****
148 c   mode search completed
149 c   order zeros found by order of increasing real part.
150 c*****
151 c
152      if(nrmode .gt. 1) then
153          jkend=nrmode-1
154
155          do 420 jk=1,jkend
156              nend=nrmode-jk
157
158              do 410 ja=1,nend
159                  nrj=nrmode-ja
160                  nrj1=nrj+1
161                  if(dimag(zeros(nrj1)).lt.
162 $              dimag(zeros(nrj))) then
163                      ctemp=zeros(nrj1)
164                      zeros(nrj1)=zeros(nrj)
165                      zeros(nrj)=ctemp
166                  end if
167 410          continue
168 420          continue
169          end if
170 c
171 c*****
172 c   the possibility exists that duplicate (within the tolerance 'tol')
173 c   zeros of the modal equation will be found.  eliminate these
174 c   duplicate zeros.
175 c*****
176 c
177      jkflag=0
178      jkend=nrmode-1
179
180      do 240 jk=1,jkend
181          jk1=jk+1
182          ctemp=zeros(jk1)
183          chksq=csubs(zeros(jk-jkflag)-ctemp)
184          if(chksq .lt. tol) then
185              jkflag=jkflag+1
186              go to 240
187          end if
188          zeros(jk1-jkflag)=ctemp
189 240      continue
190      nrmode=nrmode-jkflag

```

```

191 c
192 c*****
193 c Store the zeros as the eigenvalues.
194 c*****
195 c
196     nrmode=min0(nrmode,mxmode)
197
198     do 430 jk=1,nrmode
199         qeigen(jk)=zeros(jk)
200 430 continue
201 c
202     i1=int(r11)+1
203     if (i1 .lt. in) then
204         r1=r11+1.d0
205         call findfx(r1,t0,fx1,x1,y1,tmesh)
206         go to 50
207     endif
208     return
209 c
210 c-----
211 c                      format statements
212 c-----
213 1000 format(/5x,'searching for zeroes in this areas are',
214 $ ' defined by:/5x,'istart= ',i10/5x,'itop= ',i10,
215 $ 5x,' ibot= ',i11/5x,'ileft= ',i10,5x,'iright= ',i10)
216
217 1001 format(5x,i4,' new zeroes found in this area.')
```

```

218
219 1002 format(/5x,'*****      start search for modal eigenvalues',
220 $ '          *****')
221
222 1003 format(/5x,'tmesh= ',d15.5,5x,'tol= ',d15.5)
223
224     end
225 c
226 c
227 c*****
228 c*****
229 c
230     subroutine fzerox(t0,r1,r11,fx1,x1,y1,fx2,x2,y2,zeros,nrold,
231 $                     nrnew,tmsh0)
232 c
233 c*****
234 c fzerox is a routine for finding the zeroes of a complex function, f,
235 c which lie within a specified rectangular region of the
236 c complex q11 plane, assuming that the function has only
237 c simple zeroes over this rectangle.
238 c
239 c parameters specifying the search rectangle:
240 c     tmesh - set equal to about half the average spacing between
```

```

241 c      zeroes within the rectangle. A smaller value may be used
242 c      as a safety measure, but too small a value will result
243 c      in excessively long run time.
244 c      zeros - output list of (complex) values of q11 at which
245 c      zeroes are found.
246 c      nmew,nrold- the number of zeroes found
247 c
248 c      subroutines called--
249 c          findfx
250 c          roots
251 c*****
252      implicit double precision (a-h,o-z)
253      complex*16 f10,f01,f11,fx1,fx2,fx00,fx10,fx01,fx11,
254      +          one,sol,zeros
255      parameter(one=(1.d0,0.d0))
256 $include: 'mlaparm.inc'
      ***** Begin listing of: mlaparm.inc
1 c
2 c      include file to define the
3 c          maximum # of layers (mxlayr)
4 c          maximum # of modes (mxmode)
5 c
6      parameter (mxlayr=35 )
7      parameter (mxmode=127 )
      ***** End listing of: mlaparm.inc
257      dimension sol(3),theta(2),zeros(2*mxmode+1),rline(2,1024)
258 c
259      common/tmccom/tmesh
260 c*****
261 c
262      npoint=0
263      nmew=nrold
264      tmesh=tmsh0
265      bot=0.d0
266      t=t0-1.d0
267      r11=r1
268      r=r11
269 c*****
270 c
271      fx01=fx1
272      fx01r=x1
273      fx01i=y1
274      fx11=fx2
275      fx11r=x2
276      fx11i=y2
277      go to 82
278 c
279 c*****
280 c      enter mesh square from left side or exit rectangle at right edge.
281 c

```

```

282 20  r=r+1.d0
283 21  fx01=fx11
284      fx01r=fx11r
285      fx01i=fx11i
286      fx00=fx10
287      fx00r=fx10r
288      fx00i=fx10i
289 22  continue
290      call findfx(r+1.d0,t+1.d0,fx11,fx11r,fx11i,tmesh)
291      call findfx(r+1.d0,t,fx10,fx10r,fx10i,tmesh)
292 c*****
293 c    Determine the edge of exit of im(f)=0 from current mesh.
294      edgeit=fx01i*fx11i
295      edgeib=fx00i*fx10i
296      if (edgeib .gt. 0.d0) then
297 c        Im(f)=0 goes through the 01 to 10 line.
298          if (edgeit .gt. 0.d0) then
299 c            Im(f)=0 goes through the 10 to 11 edge (edge 1).
300              lout=1
301          else
302 c            Im(f)=0 goes through the 01 to 11 edge (edge 2)
303              lout=2
304          end if
305      else
306 c        Im(f)=0 goes through the 00 to 10 edge (edge 4)
307          lout=4
308          if (edgeit .lt. 0.d0) then
309 c            Im(f)=0 also runs through 01 to 11 and 10 to 11 edges.
310 c            Store crossing location and in/out information.
311              knot34=knot34+1
312 c              loc34r(knot34)=lr
313 c              loc34i(knot34)=li
314          end if
315      end if
316 c*****
317      go to 85
318 c*****
319 c  enter mesh square from bottom side or exit rectangle at top edge.
320 40  t=t+1.d0
321 41  fx00=fx01
322      fx00r=fx01r
323      fx00i=fx01i
324      fx10=fx11
325      fx10r=fx11r
326      fx10i=fx11i
327 42  continue
328      call findfx(r,t+1.d0,fx01,fx01r,fx01i,tmesh)
329      call findfx(r+1.d0,t+1.d0,fx11,fx11r,fx11i,tmesh)
330 c*****
331 c    Determine the edge of exit of im(f)=0 from current mesh.

```



```

332     edgeil=fx00i*fx01i
333     edgeir=fx10i*fx11i
334     if (edgeir .gt. 0.d0) then
335 c       Im(f)=0 goes through the 00 to 11 line.
336         if (edgeil .gt. 0.d0) then
337 c           Im(f)=0 goes through the 01 to 11 edge (edge 2)
338             lout=2
339         else
340 c           Im(f)=0 goes through the 00 to 01 edge (edge 3).
341             lout=3
342         end if
343     else
344 c       Im(f)=0 goes through the 10 to 11 edge (edge 1)
345         lout=1
346         if (edgeil .lt. 0.d0) then
347 c           Im(f)=0 also runs through 00 to 01 and 01 to 11 edges.
348 c           Store crossing location and in/out information.
349             knot41=knot41+1
350 c           loc41r(knot41)=lr
351 c           loc41i(knot41)=li
352         end if
353     end if
354 c*****
355     go to 85
356 c*****
357 c enter mesh square from right side or exit rectangle at left edge.
358
359 60    r=r-1.d0
360 61    fx11=fx01
361    fx11r=fx01r
362    fx11i=fx01i
363    fx10=fx00
364    fx10r=fx00r
365    fx10i=fx00i
366 65    continue
367    call findfx(r,t+1.d0,fx01,fx01r,fx01i,tmesh)
368    call findfx(r,t,fx00,fx00r,fx00i,tmesh)
369 c*****
370 c Determine the edge of exit of im(f)=0 from current mesh.
371     edgeit=fx01i*fx11i
372     edgeib=fx00i*fx10i
373     if (edgeit .gt. 0.d0) then
374 c       Im(f)=0 goes through the 01 to 10 line.
375         if (edgeib .gt. 0.d0) then
376 c           Im(f)=0 goes through the 00 to 01 edge (edge 3).
377             lout=3
378         else
379 c           Im(f)=0 goes through the 00 to 10 edge (edge 4)
380             lout=4
381         end if

```

```

382     else
383 c       Im(f)=0 goes through the 01 to 11 edge (edge 2)
384         lout=2
385         if (edgeib .lt. 0.d0) then
386 c       Im(f)=0 also runs through 00 to 10 and 00 to 01 edges.
387 c       Store crossing location and in/out information.
388           knot12=knot12+1
389 c       loc12r(knot12)=lr
390 c       loc12i(knot12)=li
391         end if
392     end if
393 c*****
394     go to 85
395 c*****
396 c enter mesh square top side or exit rectangle at bottom edge.
397 c
398 80   t=t-1.d0
399 81   fx01=fx00
400     fx01r=fx00r
401     fx01i=fx00i
402     fx11=fx10
403     fx11r=fx10r
404     fx11i=fx10i
405 82   continue
406     call findfx(r,t,fx00,fx00r,fx00i,tmesh)
407     call findfx(r+1.d0,t,fx10,fx10r,fx10i,tmesh)
408 c
409 c*****
410 c   Determine the edge of exit of im(f)=0 from current mesh.
411 c
412 83   continue
413     edgeil=fx00i*fx01i
414     edgeir=fx10i*fx11i
415     if (edgeil .gt. 0.d0) then
416 c       Im(f)=0 goes through the 00 to 11 line.
417         if (edgeir .gt. 0.d0) then
418 c       Im(f)=0 goes through the 00 to 10 edge (edge 4)
419           lout=4
420         else
421 c       Im(f)=0 goes through the 10 to 11 edge (edge 1).
422           lout=1
423         end if
424     else
425 c       Im(f)=0 goes through the 00 to 01 edge (edge 3)
426         lout=3
427         if (edgeir .lt. 0.d0) then
428 c       Im(f)=0 also runs through 00 to 10 and 10 to 11 edges.
429 c       Store crossing location and in/out information.
430           knot23=knot23+1
431 c       loc23r(knot23)=lr

```

```

432 c      loc23i(knot23)=li
433      end if
434      end if
435 c*****
436 c      Test for there being at least one re(f)=0 line entering and
437 c      leaving the mesh square.
438 c*****
439 c
440 85      continue
441      npoint=npoint+1
442      rrr=r*tmesh
443      ttt=t*tmesh
444      rline(1,npoint)=rrr
445      rline(2,npoint)=ttt
446      if (npoint .eq. 1024) lout=5
447 c
448      if((t .lt. bot) .or. (t .gt. t0)) go to 100
449
450      if ((fx00r*fx10r .gt. 0.d0) .and. (fx01r*fx11r .gt. 0.d0)
451      + .and. (fx00r*fx01r .gt. 0.d0)) go to (20,40,60,80,100)
452      + lout
453 c*****
454 c      Compute the values of the modal function at the corners of
455 c      a mesh square to determine its Taylor series to the 3rd order
456 c      for estimating its root locations.
457 c*****
458 c
459 c      f00=one
460      f10=cdexp(fx10-fx00)-one
461      f01=cdexp(fx01-fx00)-one
462      f11=cdexp(fx11-fx00)-one
463 c
464 c***** estimate locations of zeroes by radicals*****
465 c
466      call roots(f10,f01,f11,sol,nrsol)
467 c
468      do 90 n=1,nrsol
469          ureal = dreal(sol(n))
470          uimag = dimag(sol(n))
471          if (ureal .lt. 0.d0 .or. ureal .gt. 1.0d0) go to 90
472          if (uimag .lt. 0.d0 .or. uimag .gt. 1.0d0) go to 90
473 92      theta(1)=(r+ureal)*tmesh
474          theta(2)=(t+uimag)*tmesh
475          nrnew = nrnew+1
476          zeros(nrnew)=dcmplx(theta(1),theta(2))
477 90      continue
478 c
479 c*****
480 c      continue following the phase line
481 c*****

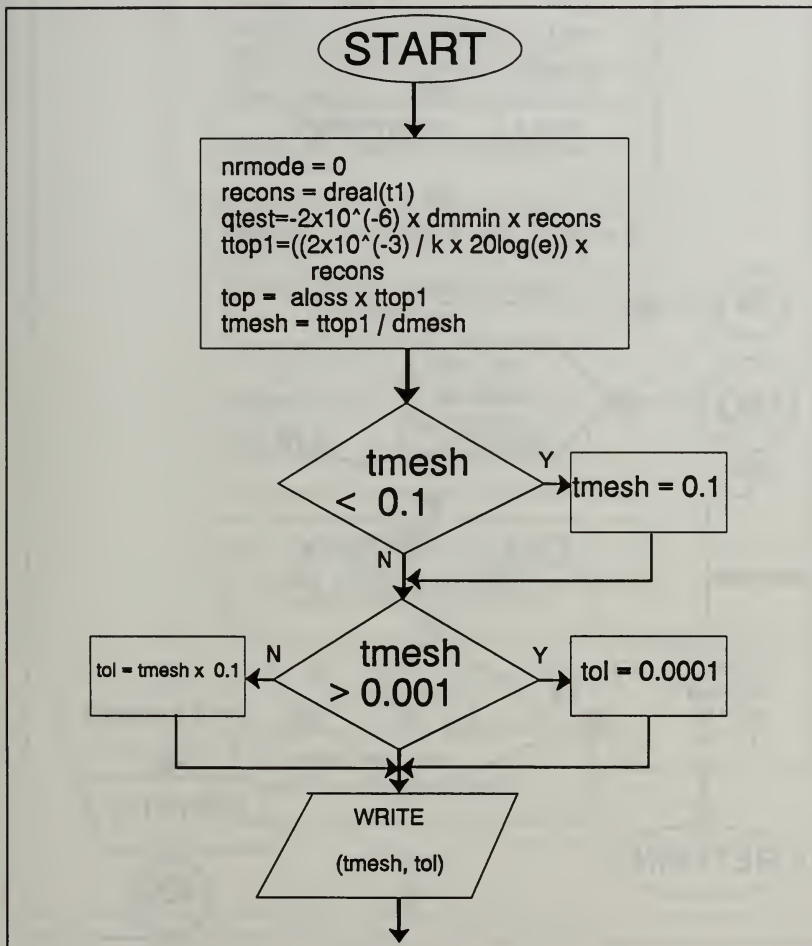
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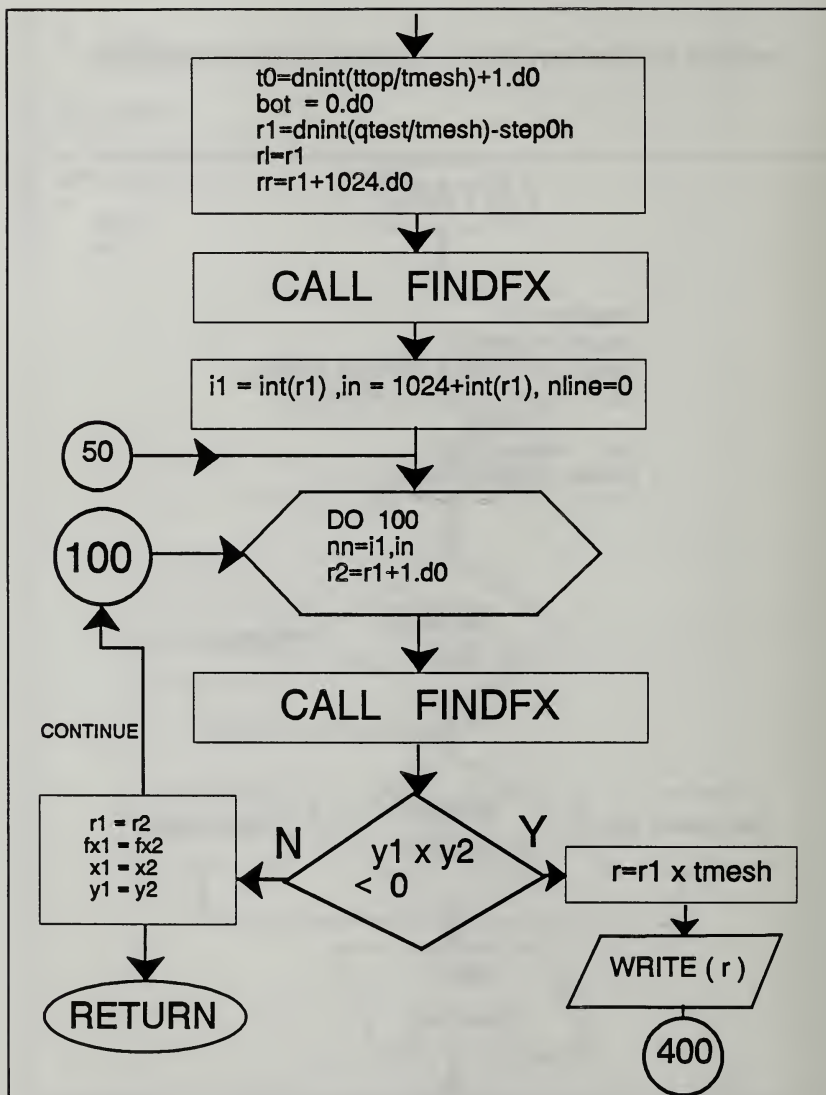
```

482 c
483 95  continue
484      go to (20,40,60,80,100) lout
485 c**
486 100  continue
487 c*****
488      write (25,8888) ((rline(i,j), i=1, 2), j=1, npoint)
489 8888  format (2e15.5)
490 c
491      return
492      end

```

# APPENDIX C: CONSTANT PHASE LINE TRACKING FLOW CHARTS





400

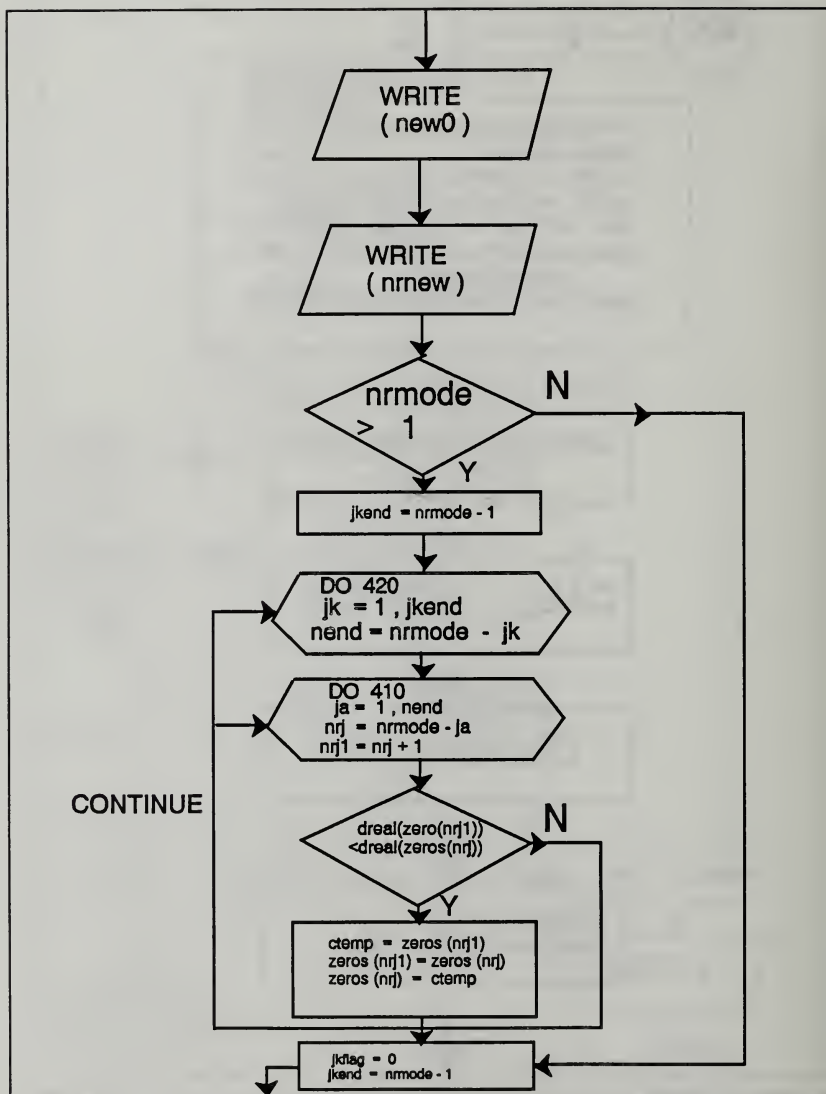
```
nroid = nrmode  
nline = nline + 1  
nc100 = int(nline/100)  
nc10 = int((nline-nc100*100)/10)  
nc1 = nline - nc100*100 - nc10*10  
kline=char(48+nc100)//char(48+nc10  
)//char(48+nc1)  
rfile='e:\ml.ch\ans\r'//filem//kline//.dat'
```

```
Open(unit=25, file=rfile, status=  
'unknown')
```

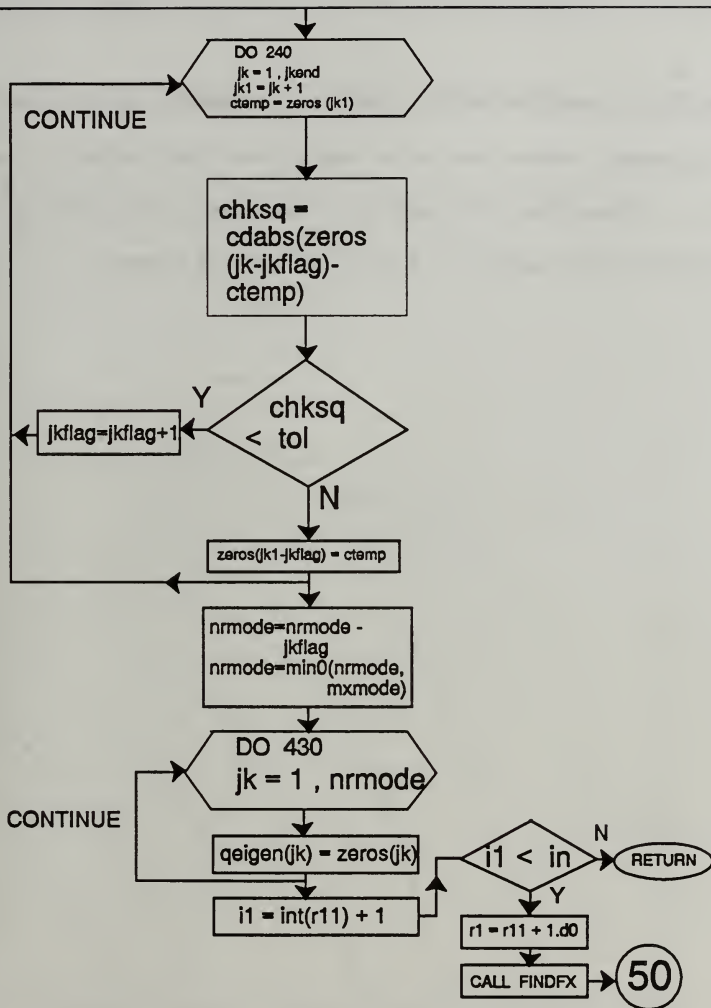
```
CALL FZEROX
```

```
CLOSE ( 25 )
```

```
nrmode = nrnew  
new0 = nrmode - nroid
```







#### APPENDIX D: CONSTANT PHASE LINES IN THE COMPLEX $q_{11}/t_1$ PLANE

This appendix contains plots of the constant phase lines  $\text{Im}\{D(q)\} = 0$  and  $\text{Re}\{D(q)\} = 0$  initiating from the top edge of the search region in the complex  $q_{11}/t_1$  plane for the evaporation ducts of 2, 4, 6, 8, 10, 20, 30, and 40 m heights.

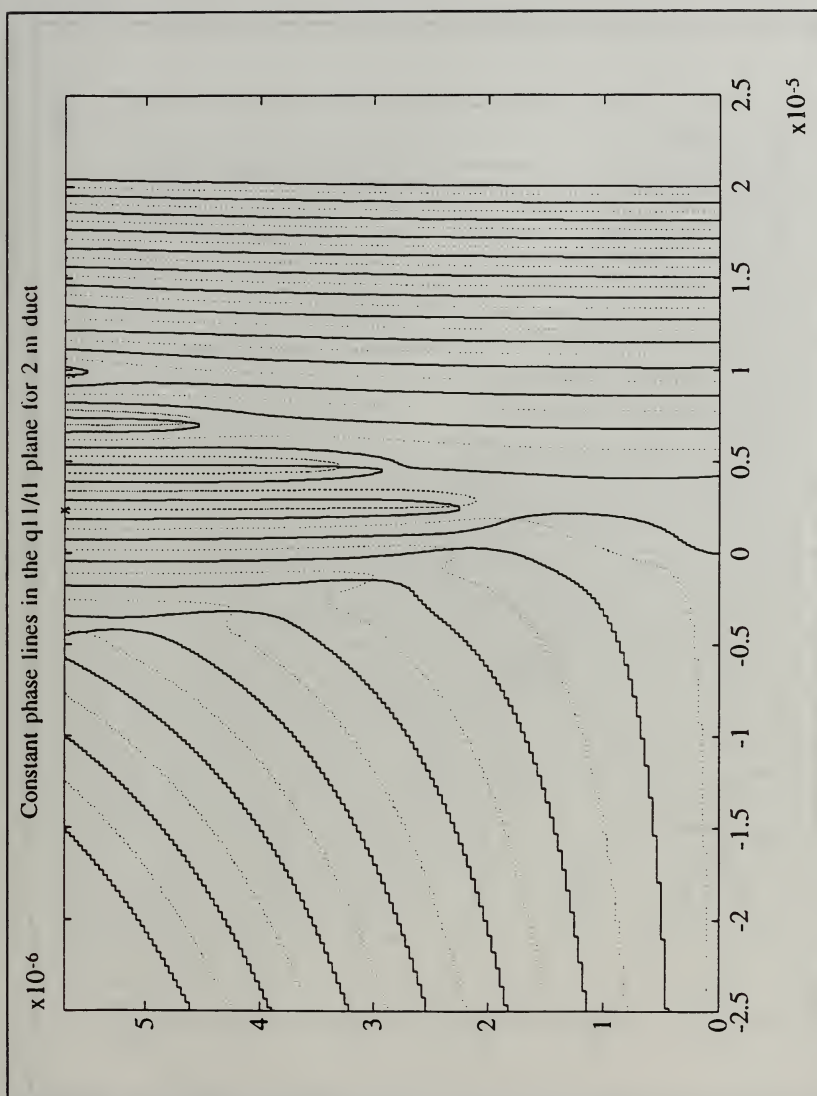


Figure D.1 Constant phase lines in the  $q_{11}/t_1$  plane (2 m duct).

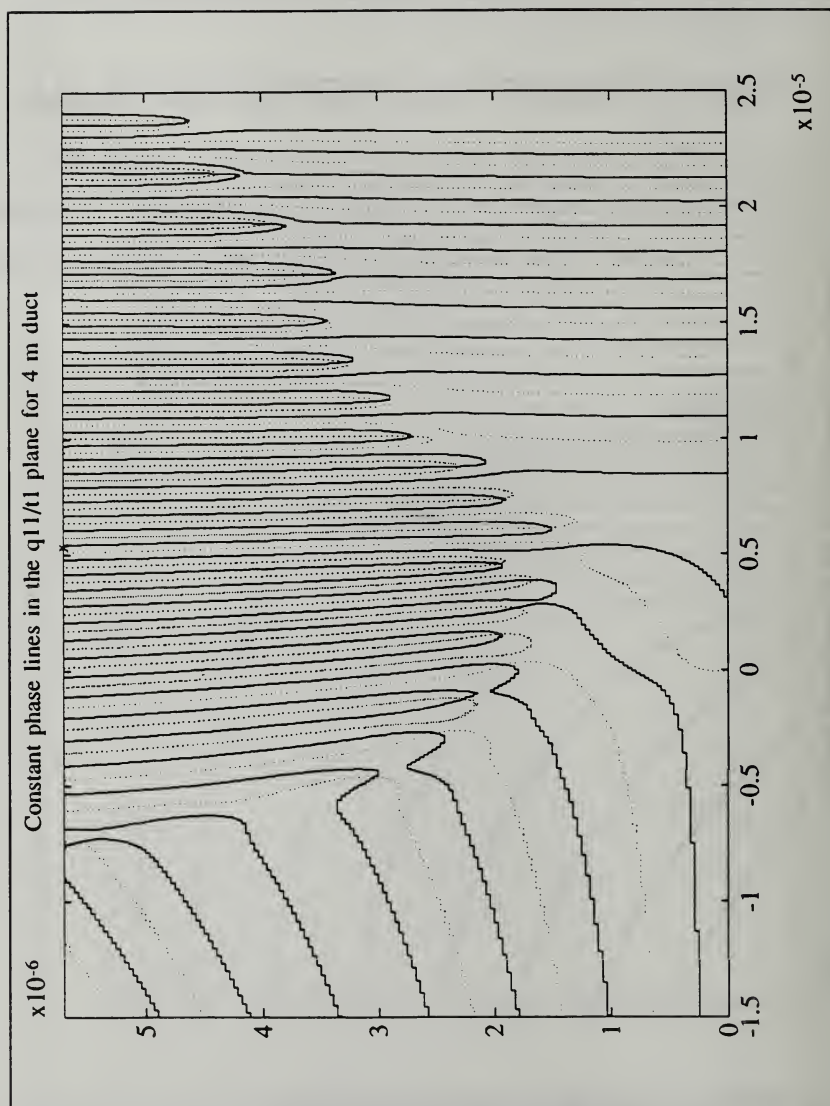


Figure D.2 Constant phase lines in the  $q_{11}/t_1$  plane (4 m duct).

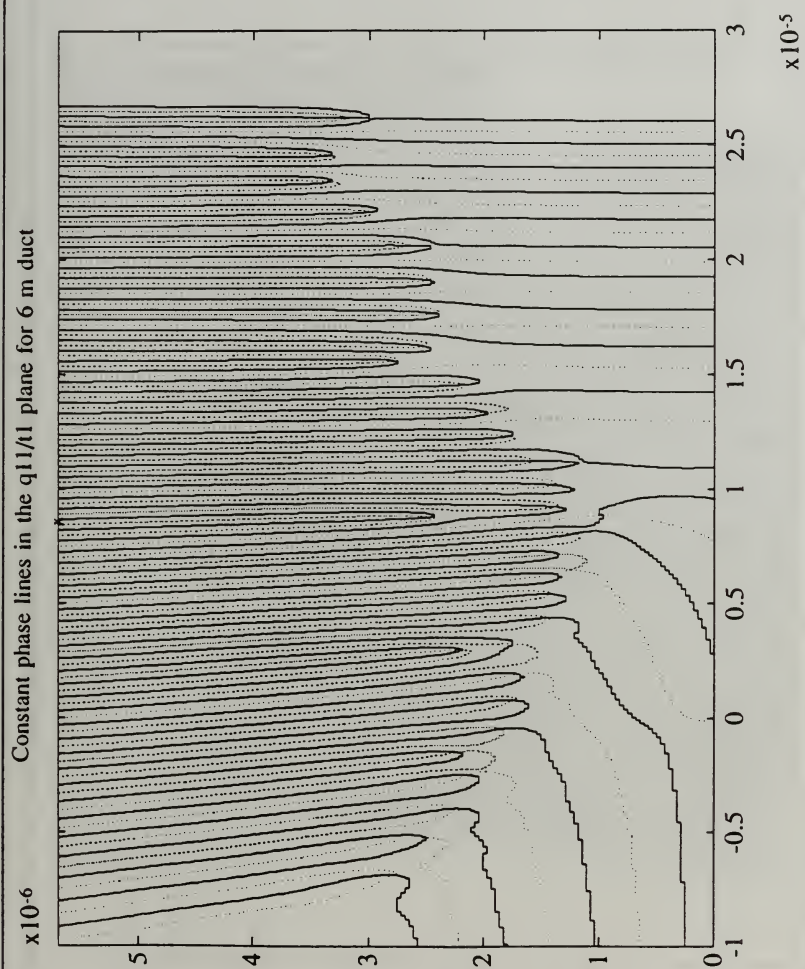


Figure D.3 Constant phase lines in the  $q_{11}/t_1$  plane (6 m duct).

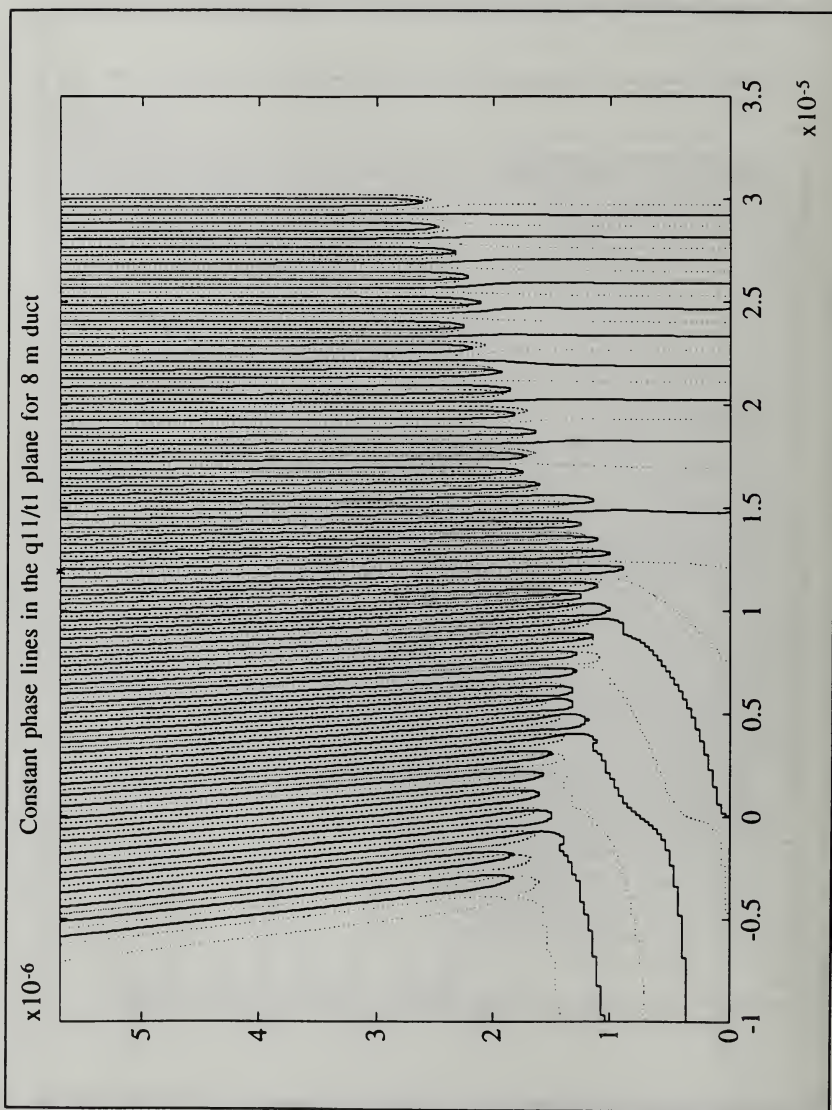


Figure D.4 Constant phase lines in the  $q_{11}/t_1$  plane (8 m duct).



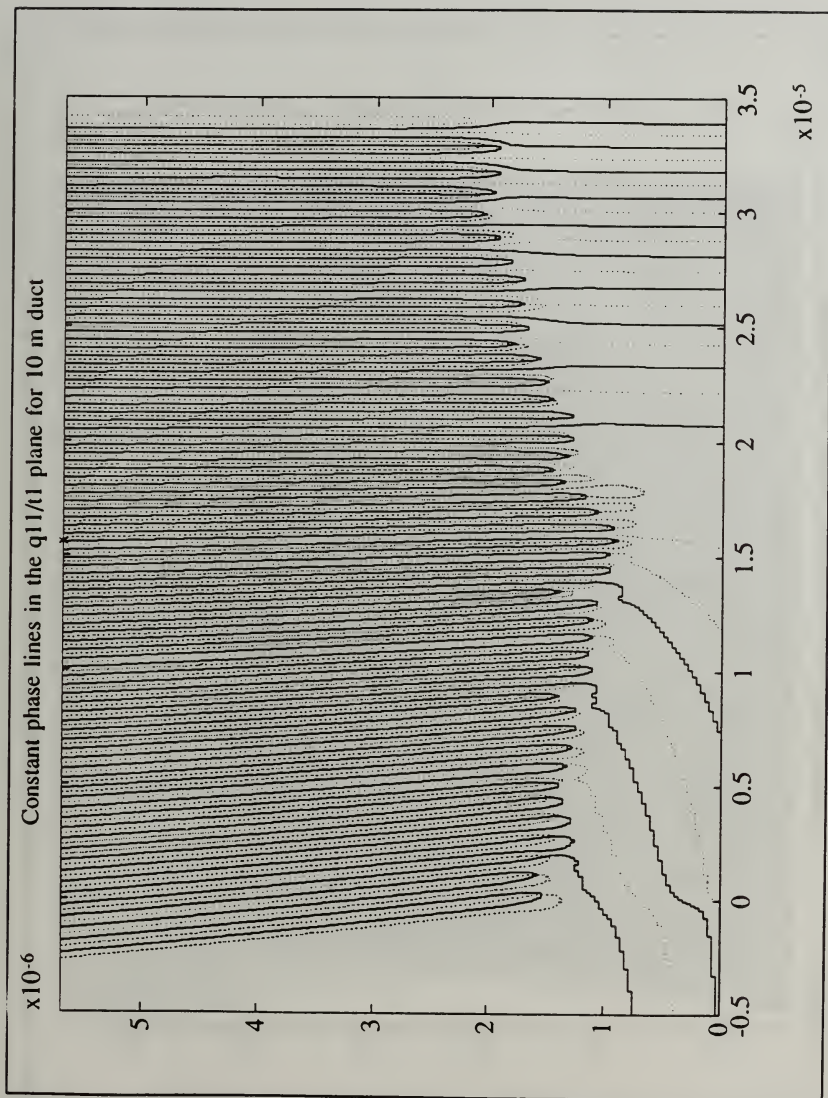


Figure D.5 Constant phase lines in the  $q_{11}/t_1$  plane (10 m duct).

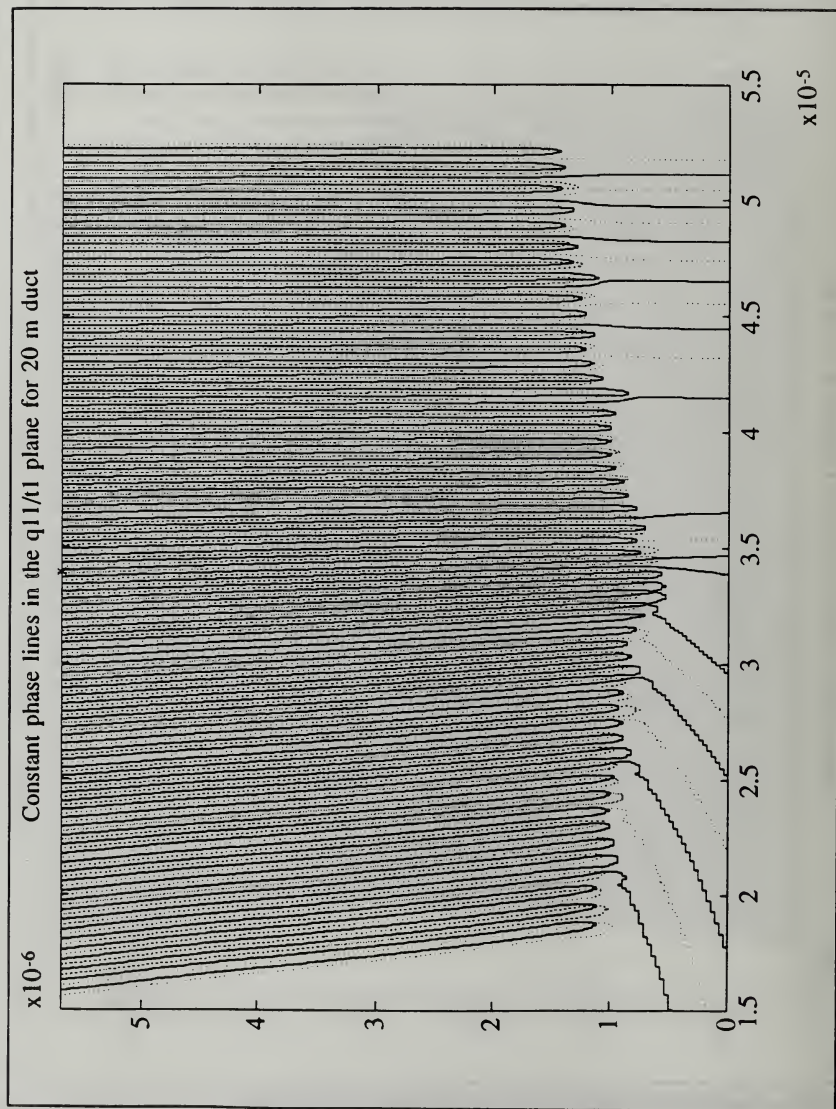


Figure D.6 Constant phase lines in the  $q_{11}/t_1$  plane (20 m duct).



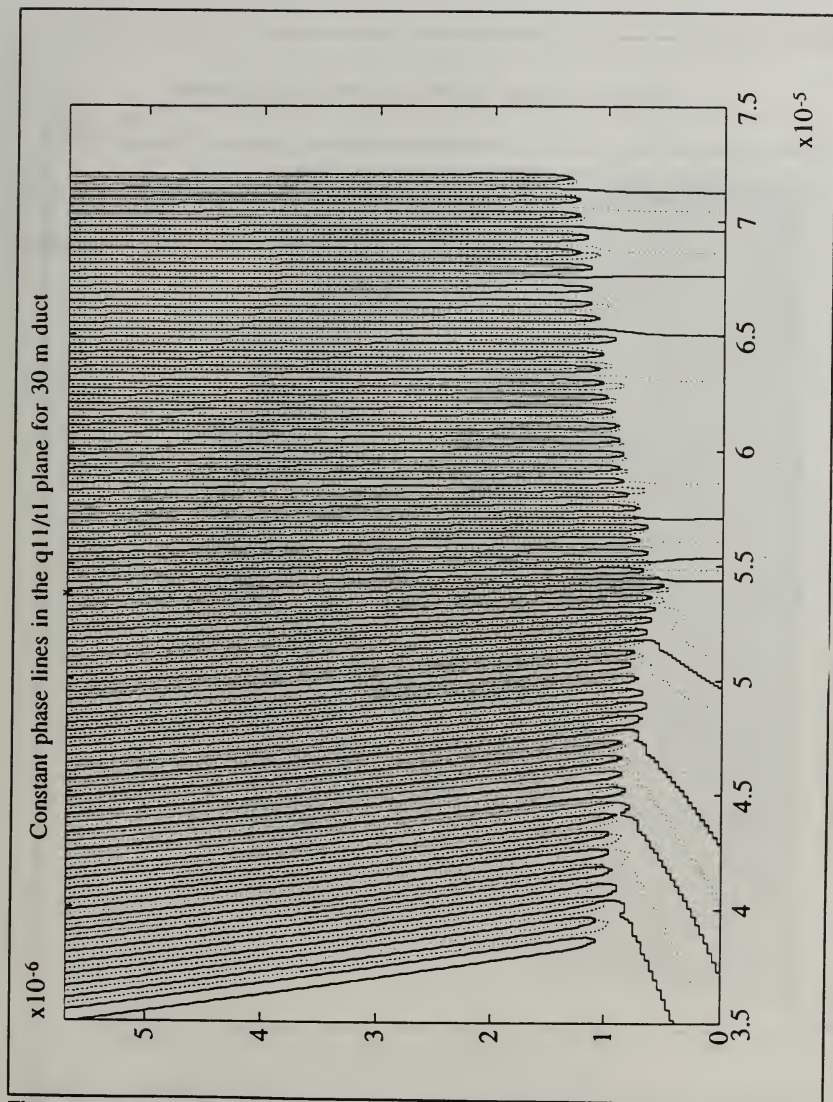


Figure D.7 Constant phase lines in the  $q_{11}/t_1$  plane (30 m duct).

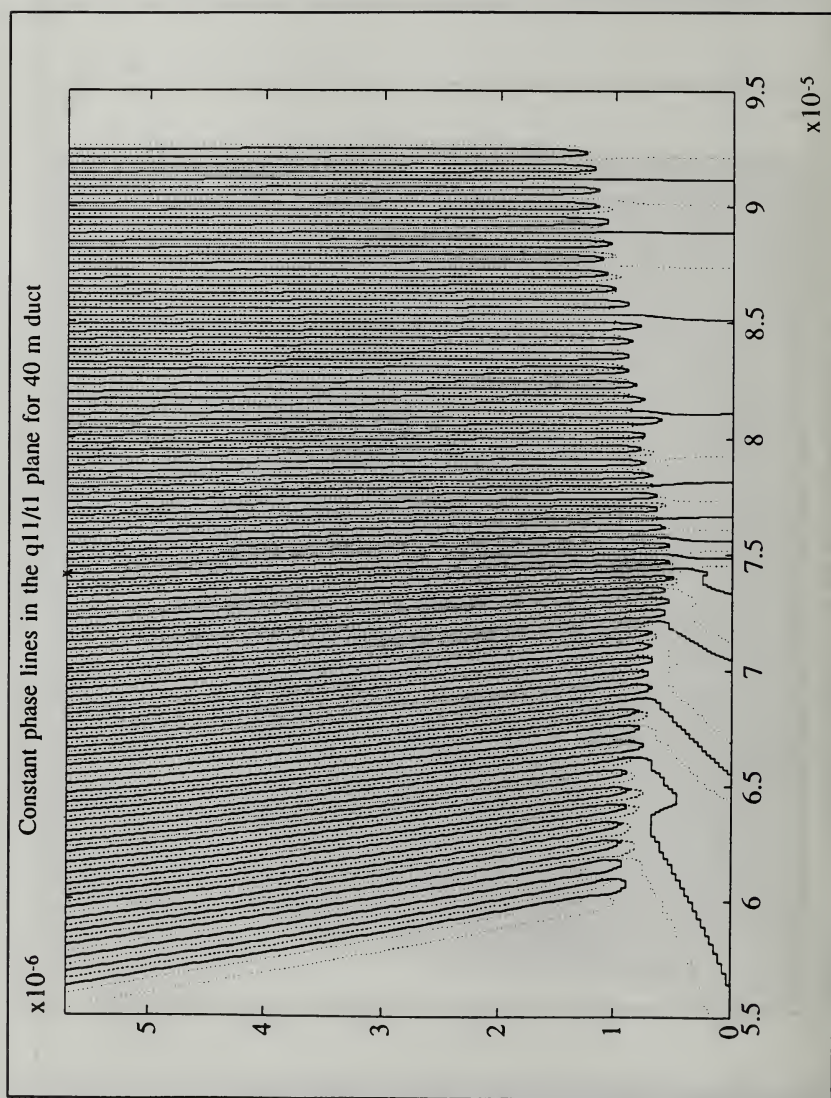


Figure D.8 Constant phase lines in the  $q_{l1}/t_1$  plane (40 m duct).

## APPENDIX E: SEPARATION OF $\text{Im}\{D(q)\}=0$ LINES

This appendix contains figures of the separation of  $\text{Im}\{D(q)\}=0$  lines along the top edge of the search region. The 2, 4, 6, 8, 10, 20, 30 and 40 meter evaporation ducts are included.

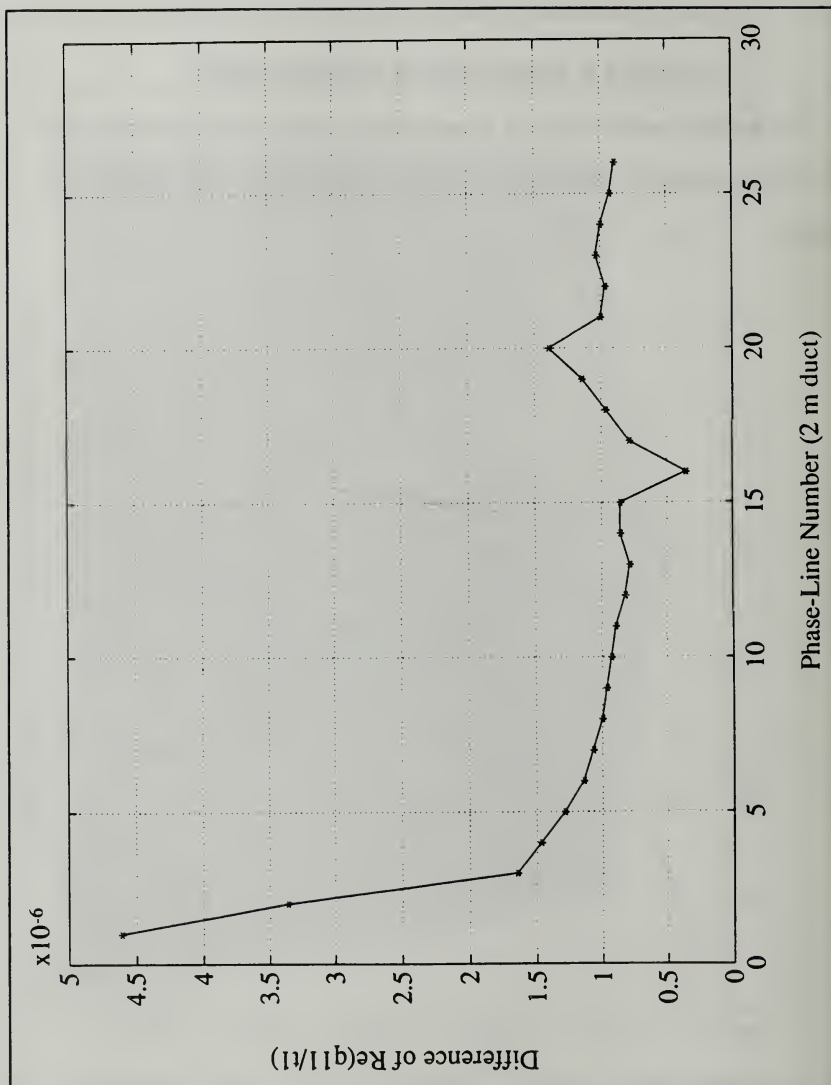


Figure E.1 Separation of  $\text{Im}\{D(q)\}=0$  lines along the top edge of the search region (2 m duct).

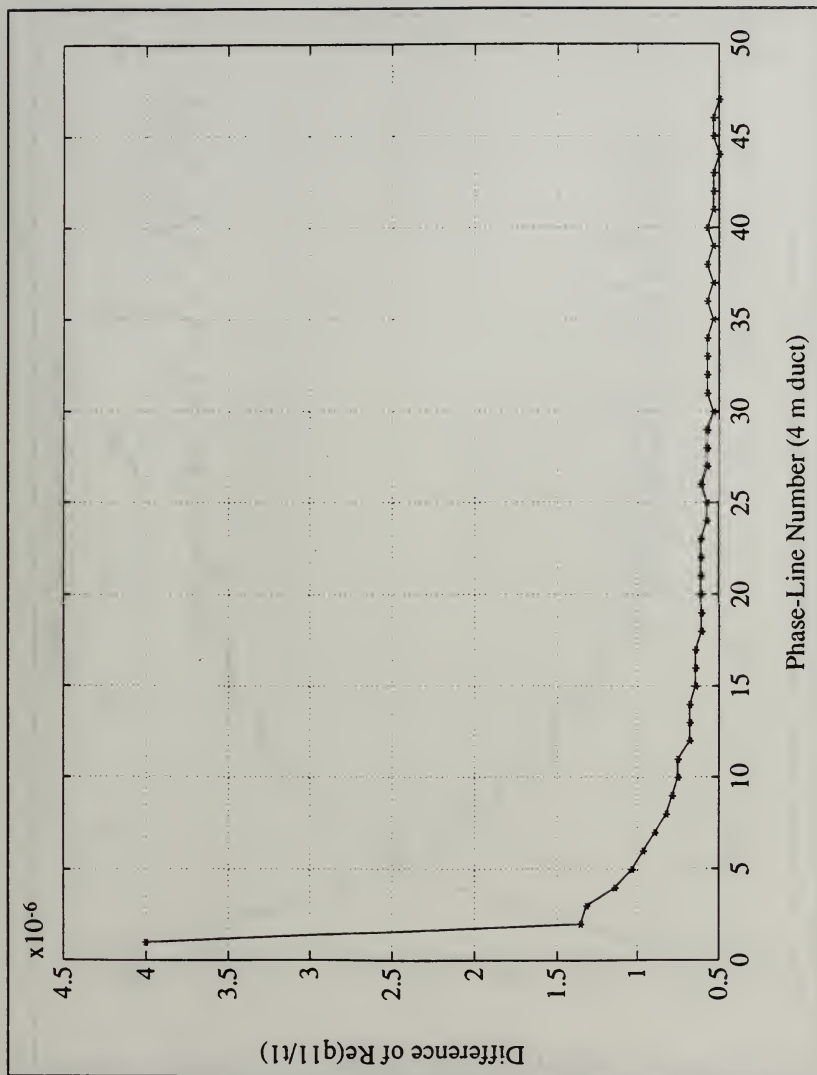


Figure E.2 Separation of  $\text{Im}\{D(q)\}=0$  lines along the top edge of the search region (4 m duct).

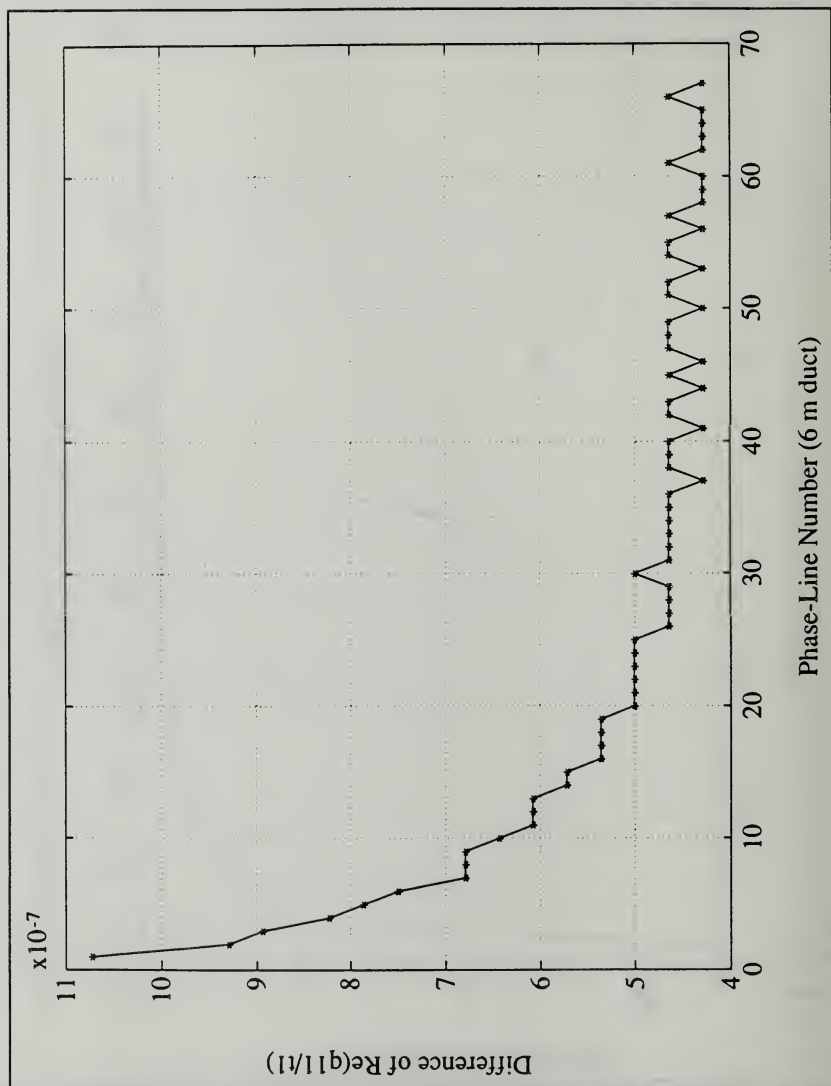


Figure E.3 Separation of  $\text{Im}\{D(q)\}=0$  lines along the top edge of the search region (6 m duct).

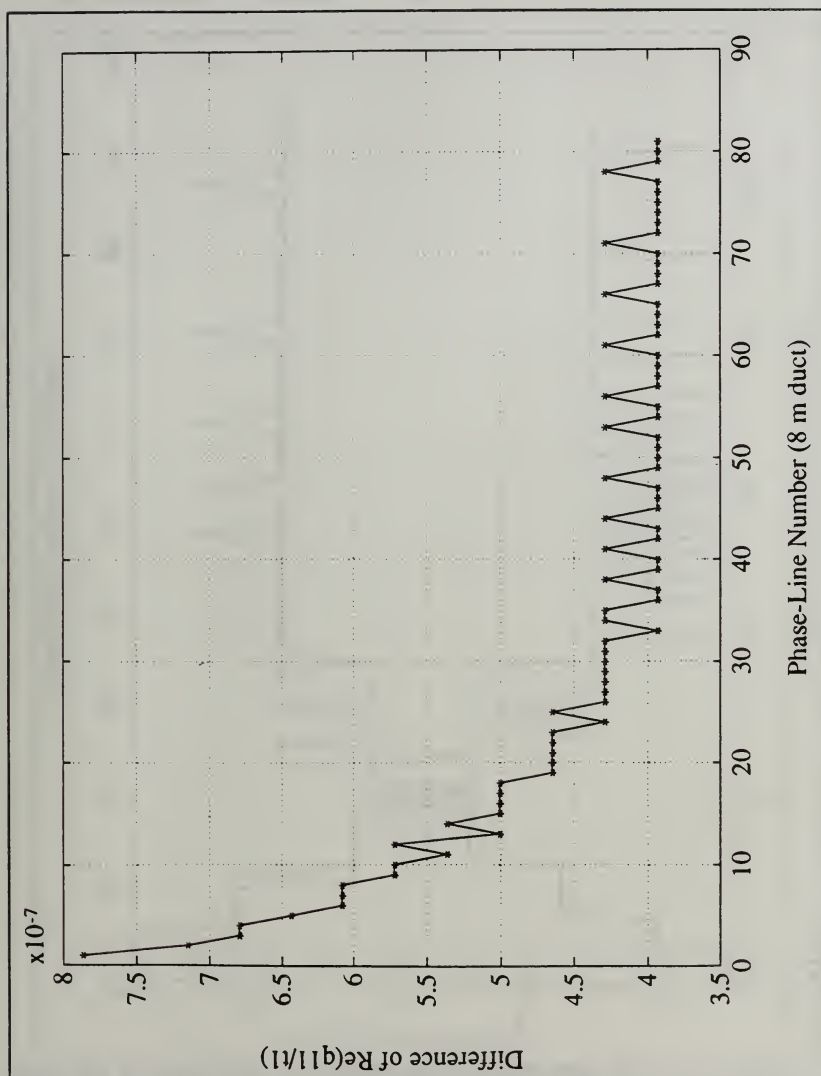


Figure E.4 Separation of  $\text{Im}\{D(q)\}=0$  lines along the top edge of the search region (8 m duct).



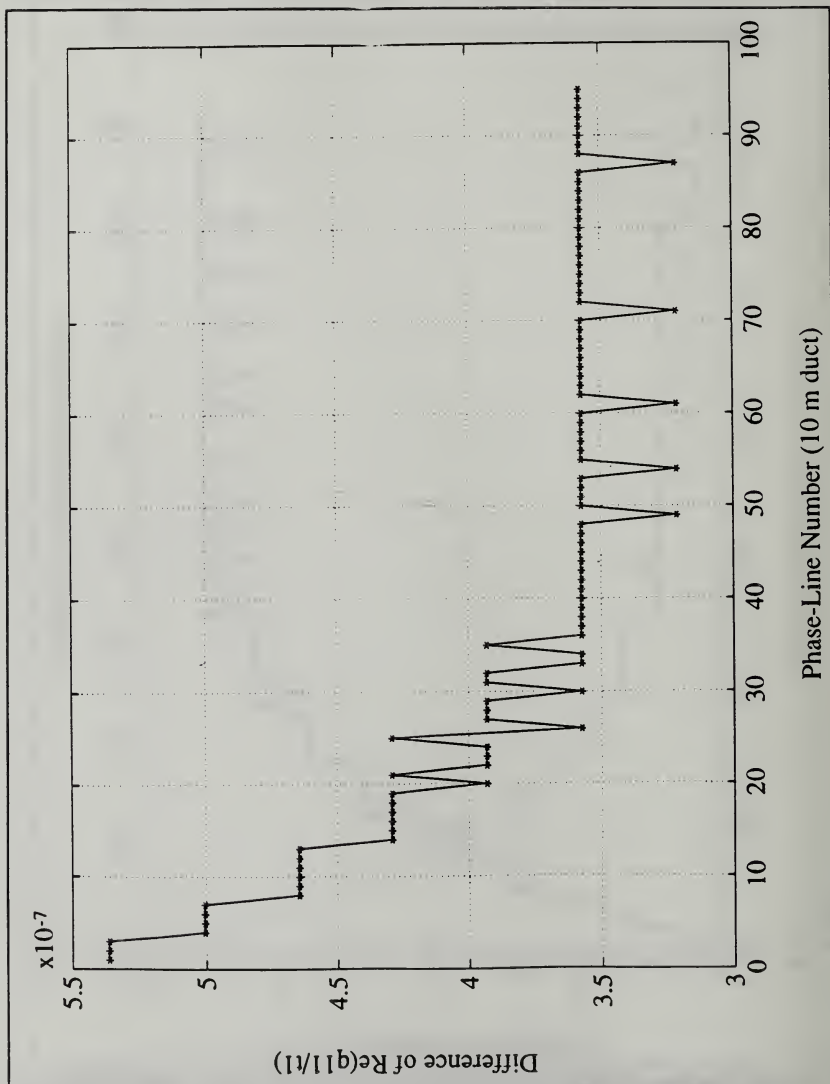


Figure E.5 Separation of  $\text{Im}\{D(q)\}=0$  lines along the top edge of the search region (10 m duct).



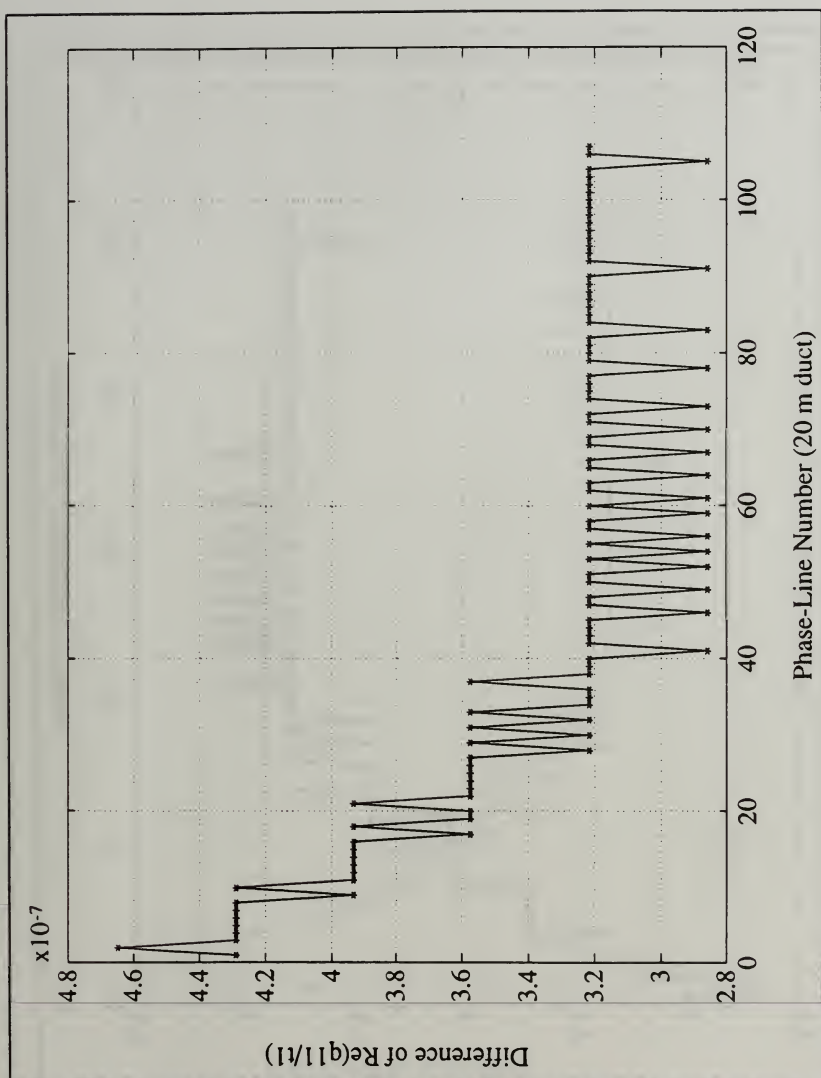


Figure E.6 Separation of  $\text{Im}\{D(q)\}=0$  lines along the top edge of the search region (20 m duct).

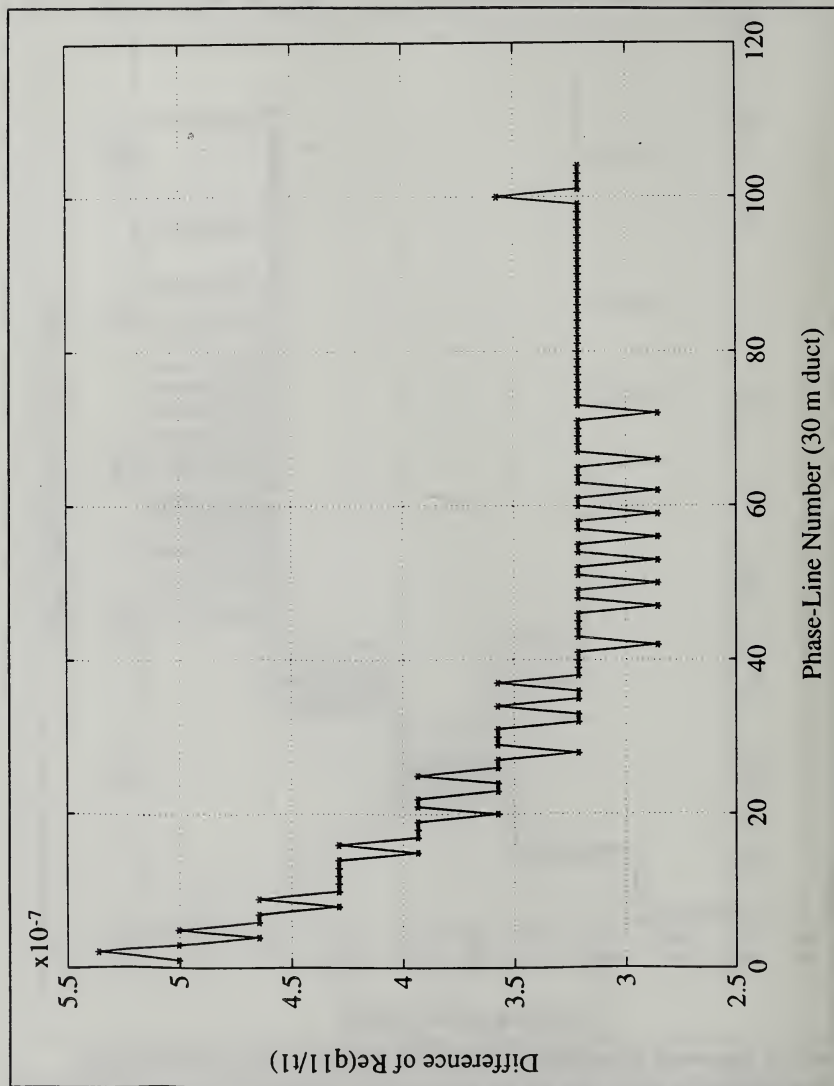


Figure E.7 Separation of  $\text{Im}\{D(q)\}=0$  lines along the top edge of the search region (30 m duct).

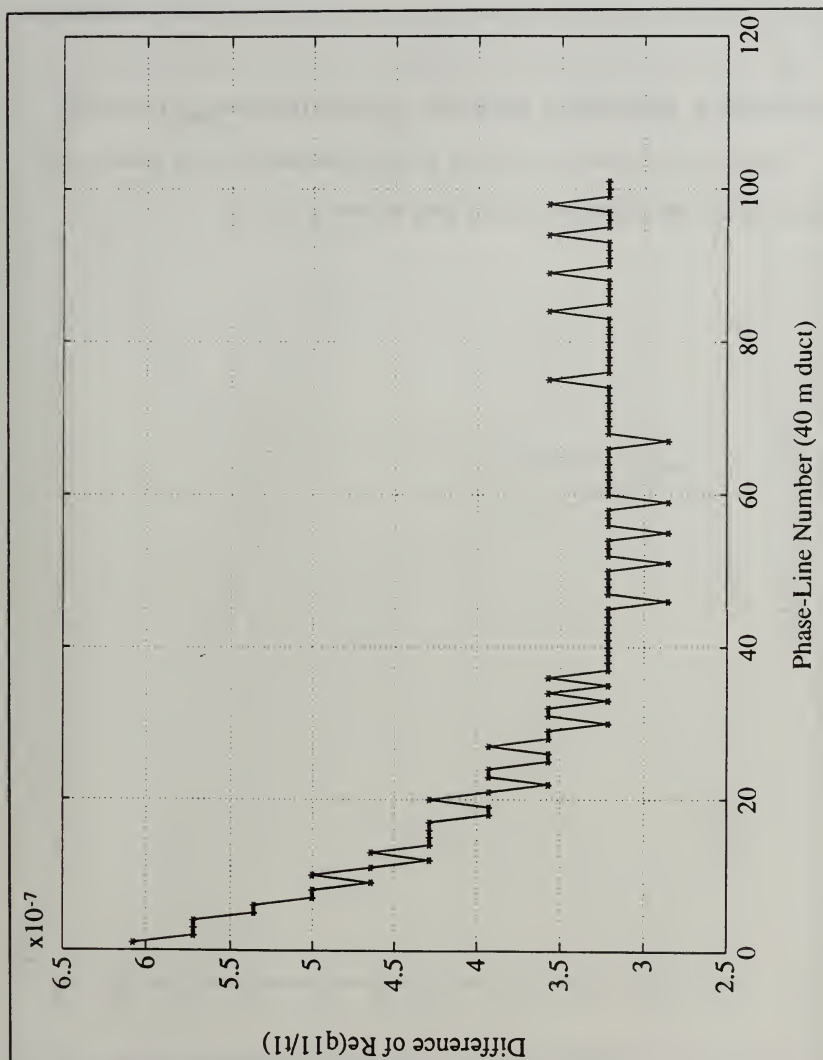


Figure E.8 Separation of  $\text{Im}\{D(q)\}=0$  lines along the top edge of the search region (40 m duct).

## APPENDIX F: DIFFERENCE BETWEEN CONSECUTIVE $\text{Re}(q_m/t_1)$ VALUES

Separation in real part of neighboring  $q$ -eigenvalues scaled by  $t_1$  is plotted in this appendix against the eigenvalue locations along the real  $q_1/t_1$  axis.

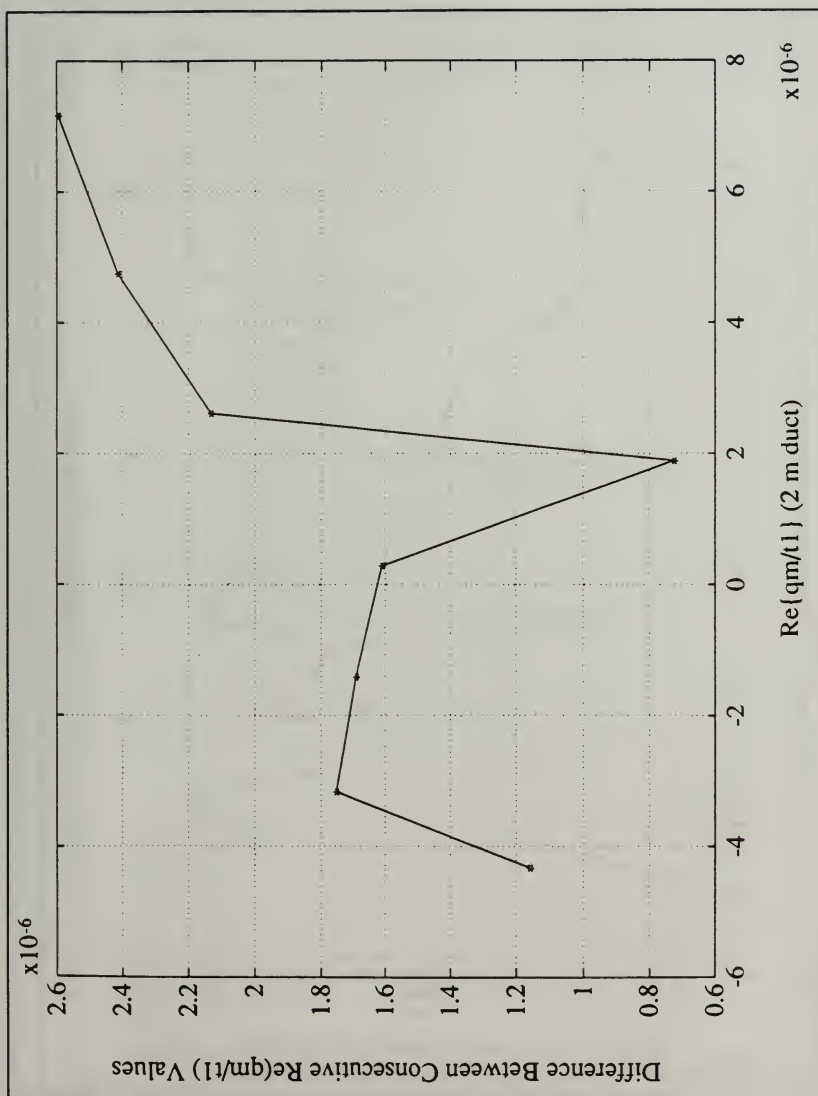


Figure F.1 Difference between consecutive  $Re(qm/t1)$  values (2 m duct).

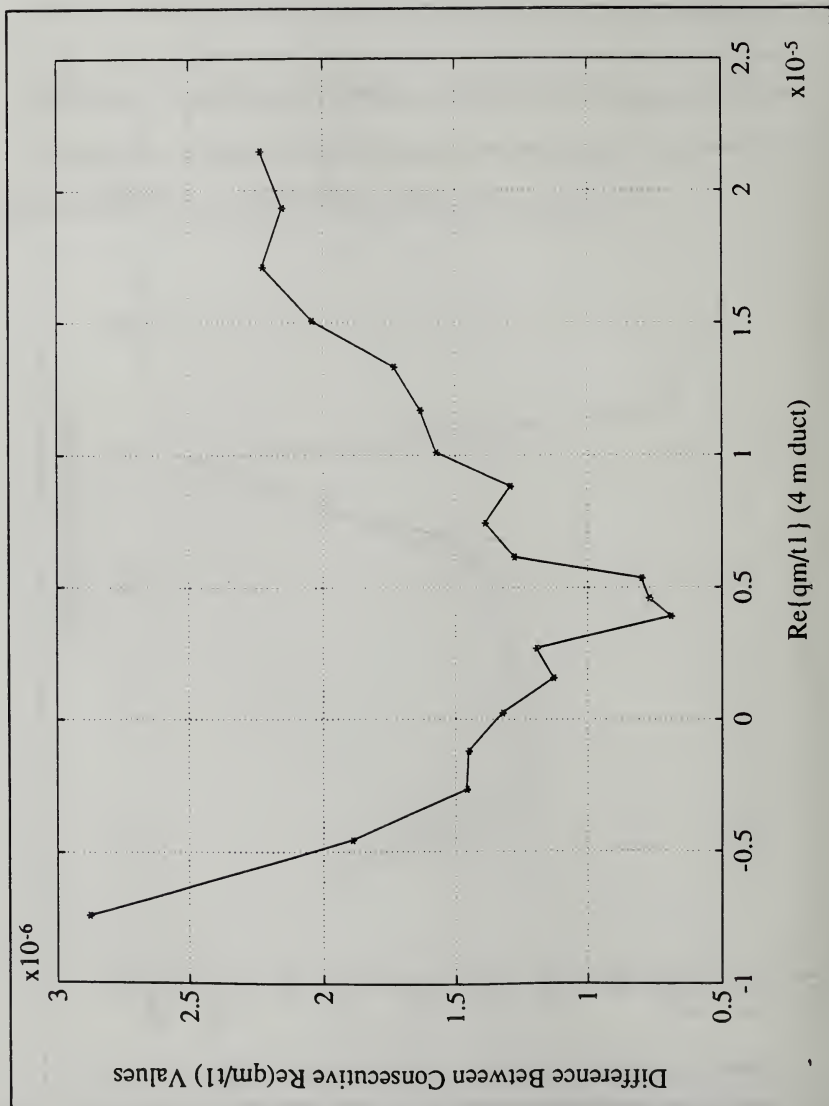


Figure F.2 Difference between consecutive  $\text{Re}(q_m/t_1)$  values (4 m duct).

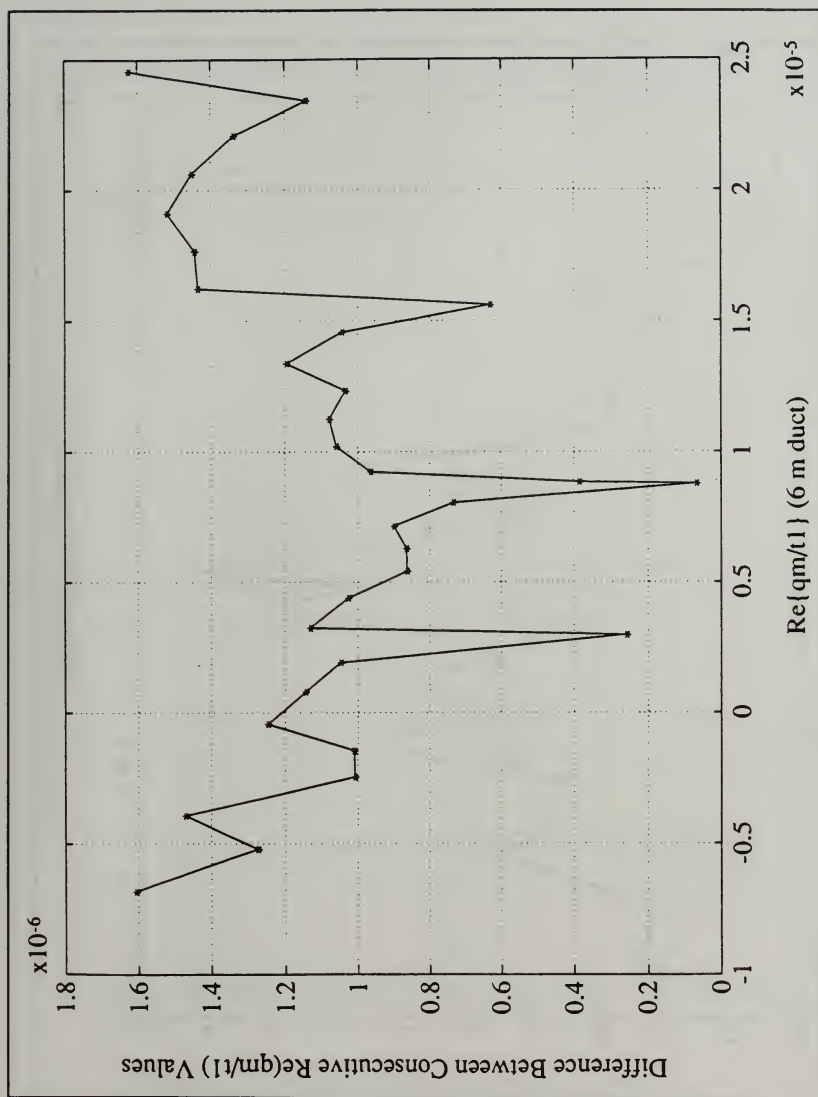


Figure F.3 Difference between consecutive  $Re(q_m/t_1)$  values (6 m duct).

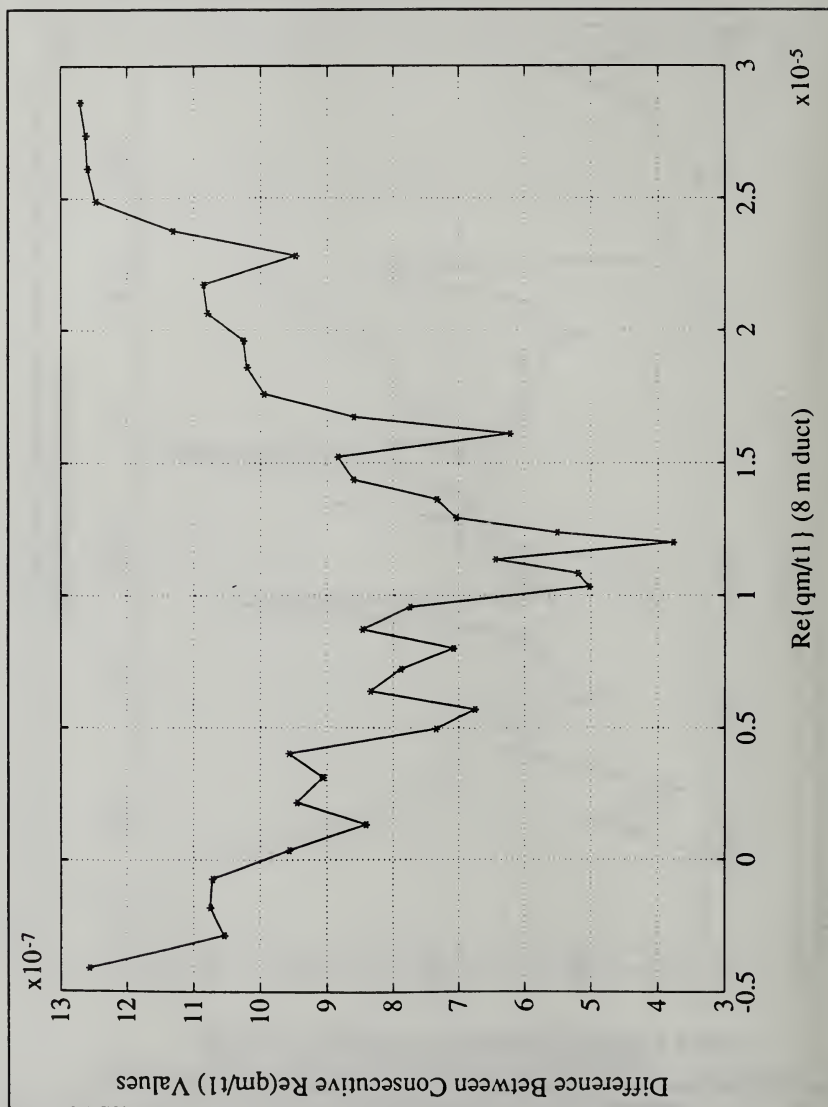


Figure F.4 Difference between consecutive  $\text{Re}(q_m/t_1)$  values (8 m duct).



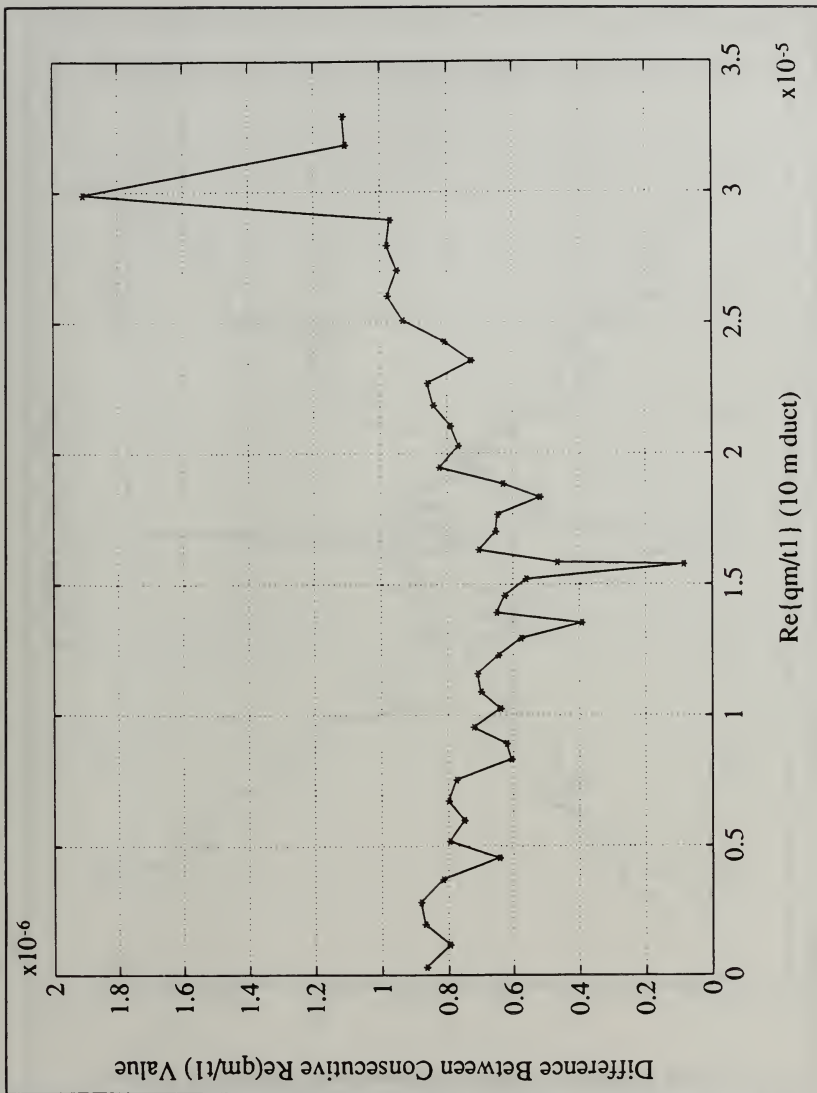


Figure F.5 Difference between consecutive  $Re(q_m/t_1)$  values (10 m duct).

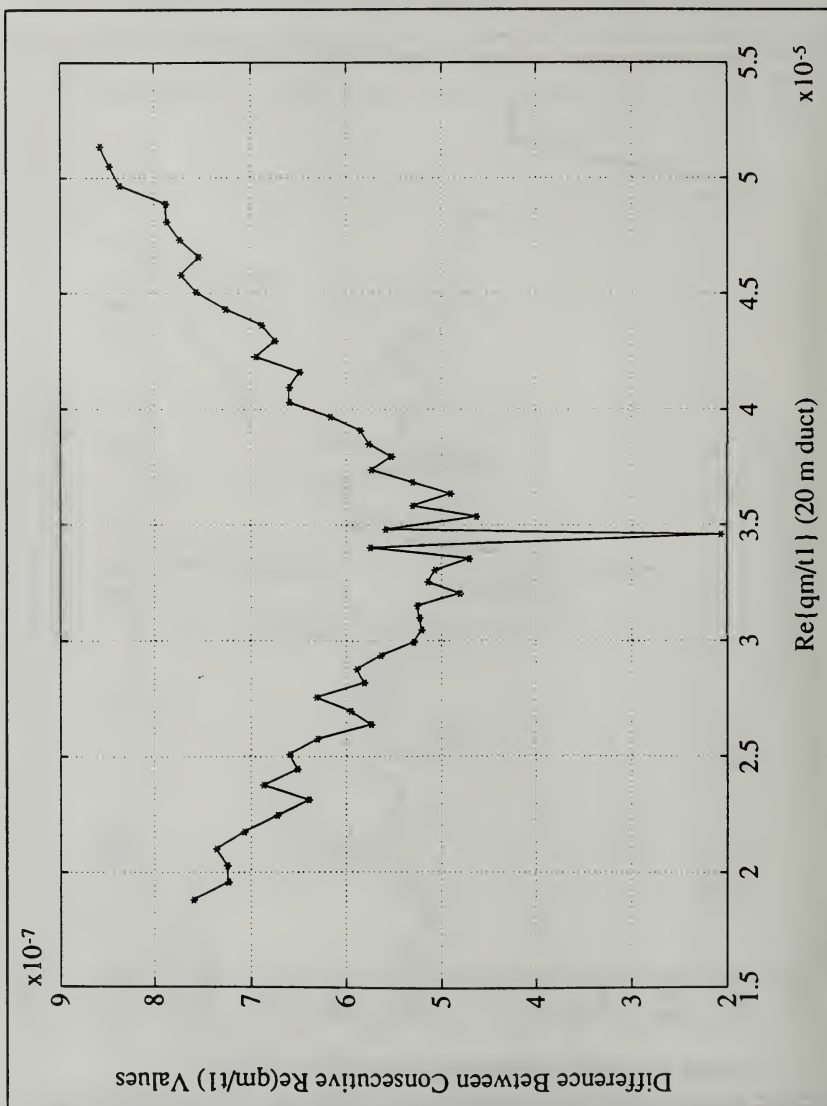


Figure F.6 Difference between consecutive  $Re(q_m/t_1)$  values (20 m duct).

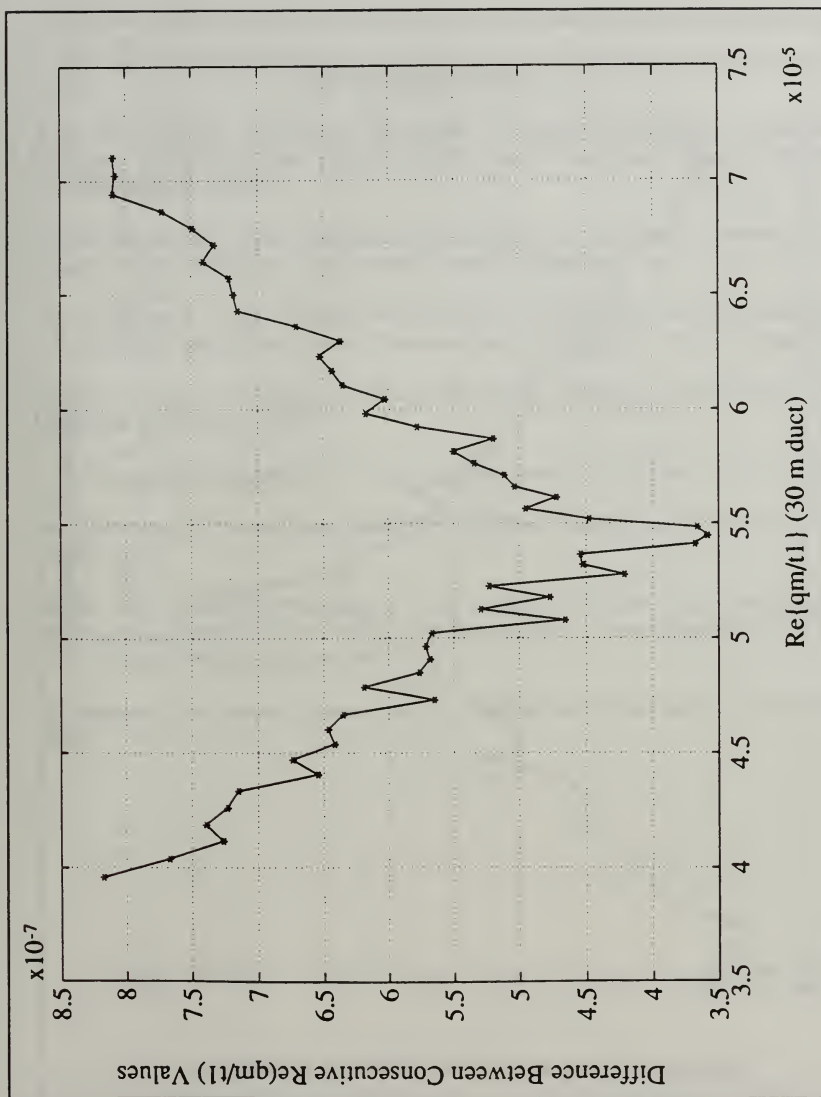


Figure F.7 Difference between consecutive  $Re(q_m/t_1)$  values (30 m duct).

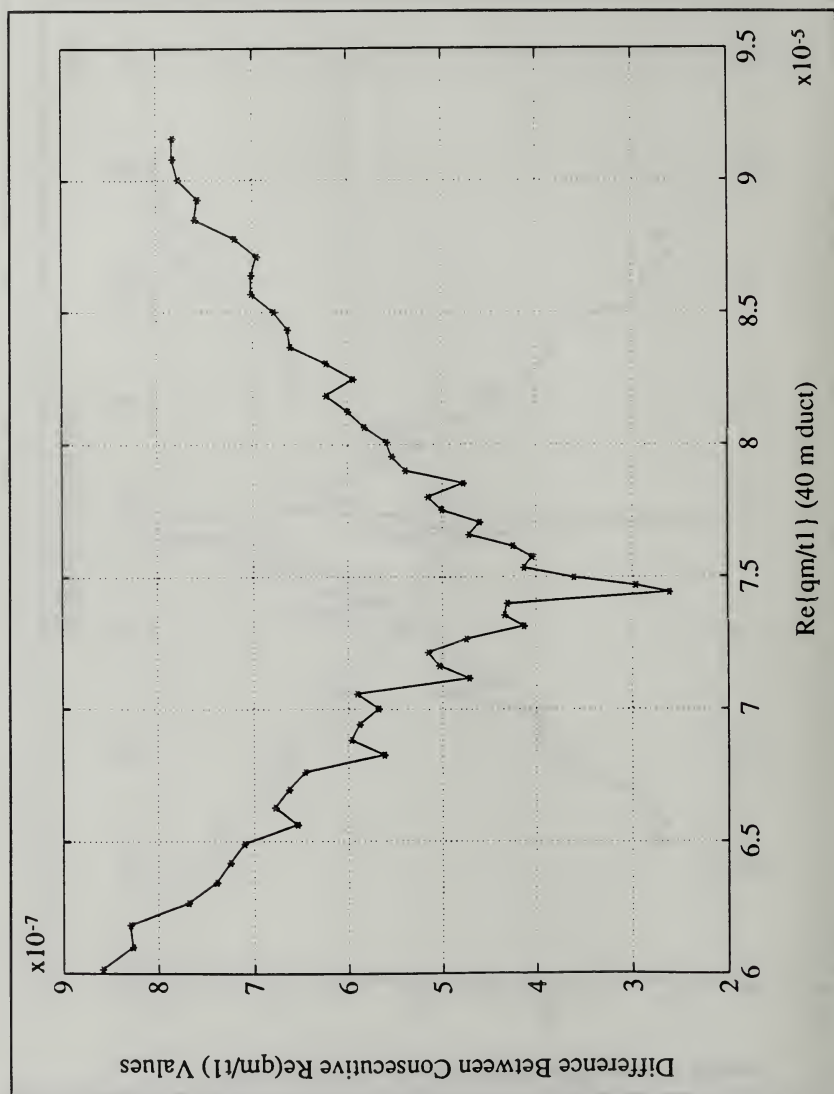


Figure F.8 Difference between consecutive  $Re(q_m/t_1)$  values (40 m duct).

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